

FIELD BOOK

S 1135

PLEASE RETURN TO  
GEAUGA COUNTY ENGINEER  
COURT HOUSE  
CHARDON, O.  
PHONE 250-X

Under Ledge Road T.H. 56 ✓  
Webster Road Pg. 21 T.H. 53 ✓  
CLAY STREET

Levels - Clay Street ± 550' N. of Thompson Rd  
Pg. 28-29 ✓

T.R. 53 J CLAY (WEBSTER) - DRAINAGE PROBLEM 9

★ SHAW'S ★

PIONEERS  
SINCE 1831

Field Book  
No. S 1135

MADE IN 88 LEAVES

A Product of Wilson-Jones Co.  
Made in U. S. A.

156

PAPER AND LITHOGRAPHING  
GUARANTEED WATERPROOF

T.H. 56

Under Ledge Road #Location  
sidestakes set 25' Lt.

8

7

6

5

4

3

2

1

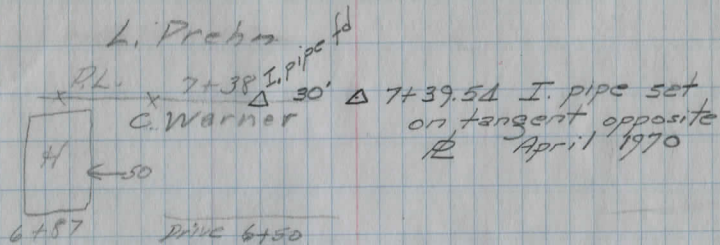
Sta 0+00 Beginning of Imp.

2 on  
tangent  
Belt set

Richey  
Clause  
Richards

3/10/38

1



C Warner

PL. x 3+37

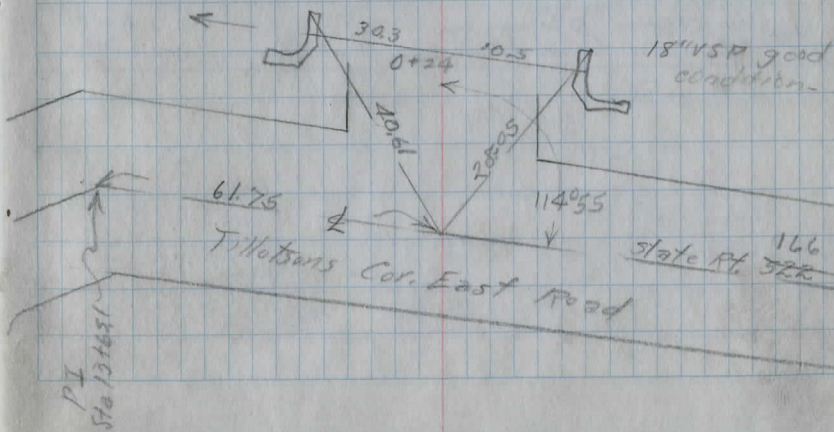
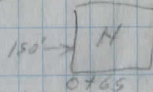
L. Prehn

2+05 DRIVE

DRIVE

ARIDIOIDE

0+95



State Rt. 166  
522

20

19

18

17

16

15

14

13

12

Sta 11+77.85 P.O.T.

Bolt  
Set

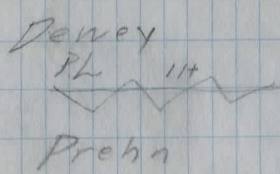
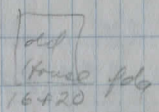
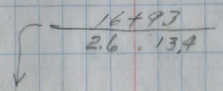
11

10

9

8

fair condition  
10° CMP  
Relocate to  
Sta 16+40



Guardian Set

25.28 S&W 12" Oak

Prehn.

56.65

S&W  
tw 8" W. Cherry

32

31

30

29

Sta 28+94.70 PI Def. Lt. 25°21' 1" Iron pin Set

28

Δ-25°21'

D-120

T-107.38

E-119

L-211.25

PC-27+87.32

PT-29+98.57

28-.1  
29-10.2

25

24

Δ-25°46'

D-10°

T-131.65

E-14.8

L-257.67

PC-20+44.73

PT-23+02.40

Version # = 2.15

21-2.6

22-8.7

23

22

Sta 21+75.38 PI Def Rt 25°46' 1" Iron Pin Set

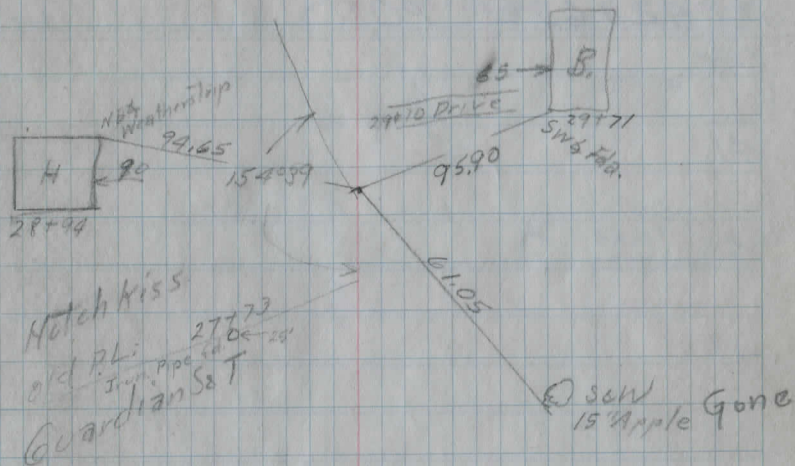
21

20

M. Judson

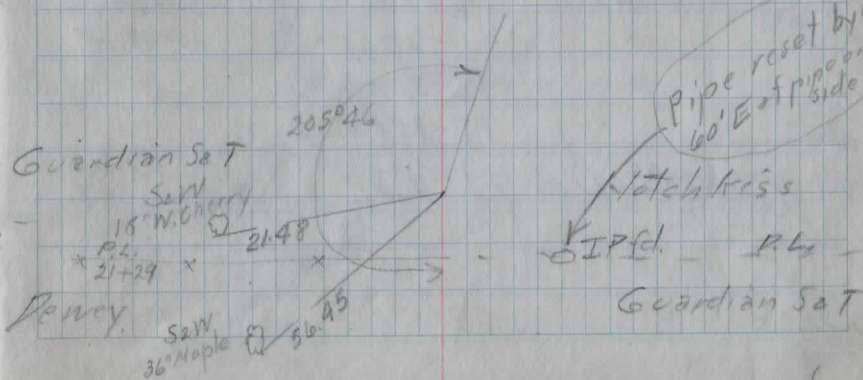
M. Judson

PLy IPd 31+47 x PLy  
1/2 x 1/2 Stone Box | 31+00 | 10.2 28 | → Hatch Kiss  
Hatch Kiss



Δ 24+23.35 I. pipe set on tangent April 1970

Pipe reset by M.R. 60' E of pipe on N. side



44

43

Sta 42+65.68 POT.

Bolt set

42

41

40

39

38

37

Δ	-7°32'	
D	-2°	32-
T	-158.60	33-21
E	-6.2	34-4.9
L	-376.67	35-.8
PC	-31+90.45	
PT	-35+67.12	

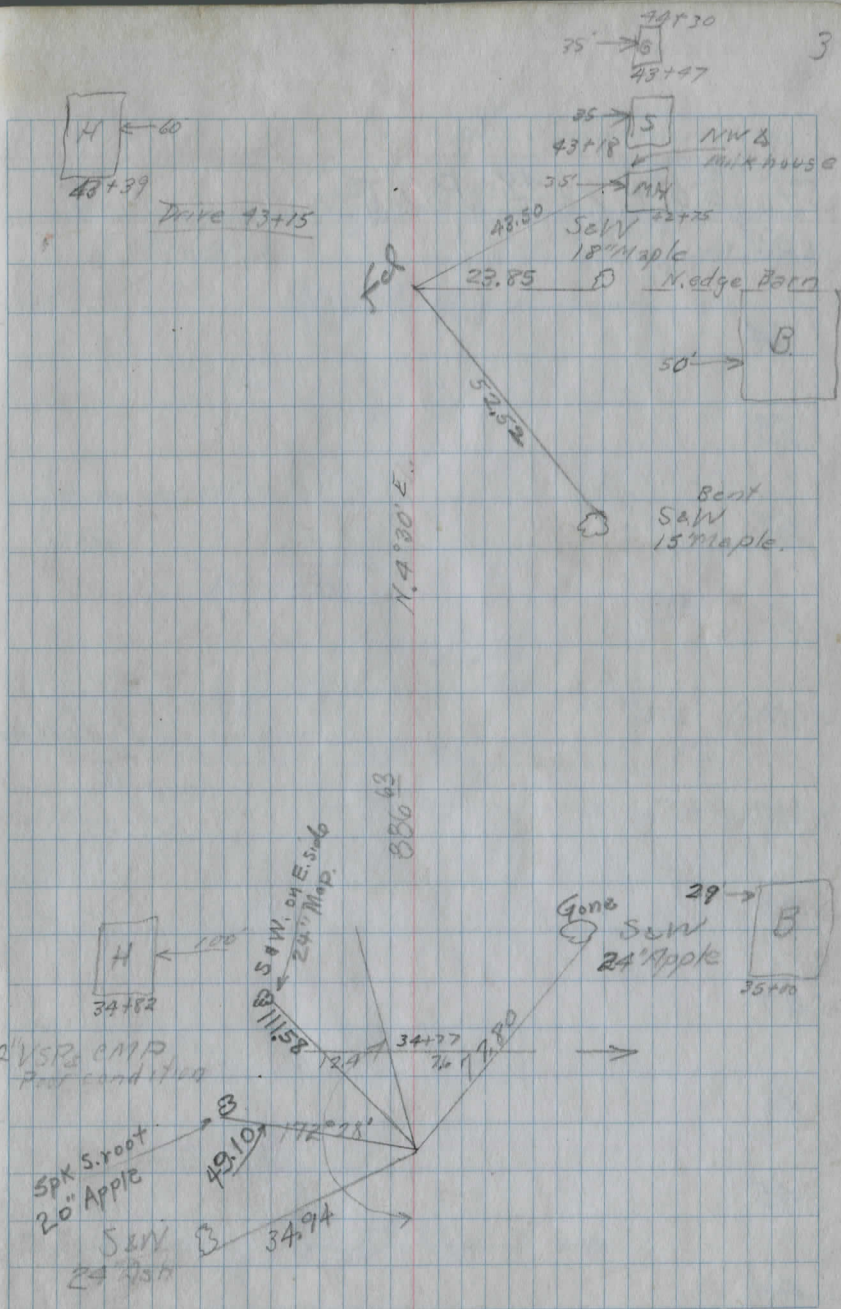
34

Sta 33+79.05 Def Lt 7°32'

Pipe set

33

32



56

Sta 56+72<sup>49</sup> P.O.T.

Bolt  
set

55

54

53

52

51

50

No road now

49

48

47

46

45

44

O Gross

PL

A Murphy

2 1/2 x 2 Stone Box

No  
fd

50.92

33.30

55+72

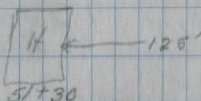
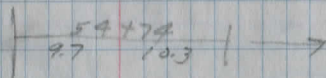
A Murphy

58W  
30° Maple

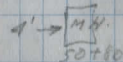
58W  
8" Pear

O Gross

PL



Drive 51+15



51+50

B

25'

A Murphy

A Murphy

Road

49+42

1 1/2 Stone Box  
poor condition

47+36  
9 8

F Harvey

1 1/2 x 1 1/2 Stone Box

46+85  
9.5 7.5

Drive 45+10

2 x 2 Stone Box  
poor condition

44+94  
19 15

68

67

66

65

Sta 64+50.28 PI Def Lt 1°10' 1" Iron Rod set

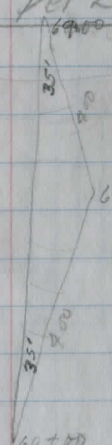
64

63

62

61

all 60 and 69  
intersection of tangents



offsets

61	1.02
62	2.04
63	3.06
64	4.08
65	4.08
66	3.06
67	2.04
68	1.02

Sta 60+00 Def. Lt. 3°35'

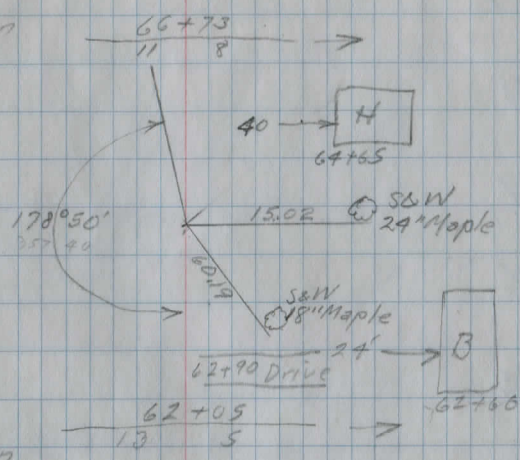
59

58

57

56

20" CIP  
Good condition

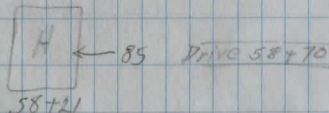


18" CIP  
Fair condition

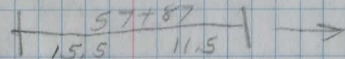
C Goodrich.

60+99x PLx

O Gross



3x2 Stone Box



80

79

78

77

76

75

74

Sta 73+68<sup>00</sup>

POT

Bolt  
Set

73

72

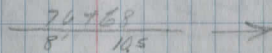
71

70

Sta 69+00 Def Lt 0°35'

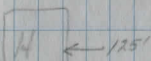
68

20" CIP good  
condition



x PL v 74+01

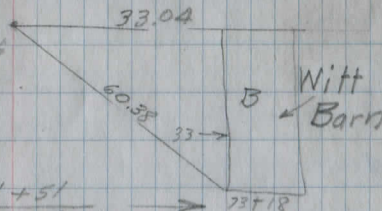
PL.?



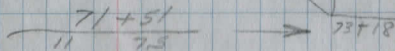
74+78 Drive 74+50

74+00 Drive

No find 5-27-40  
1/2" IP set from reference  
T.R. ROOT



15" CIP  
Poor condition



more IP

1.657 miles  
 $5250 \overline{) 8748.88}$

Sta 87+48<sup>88</sup> End of Project

Pipe  
 4d

87

86

85

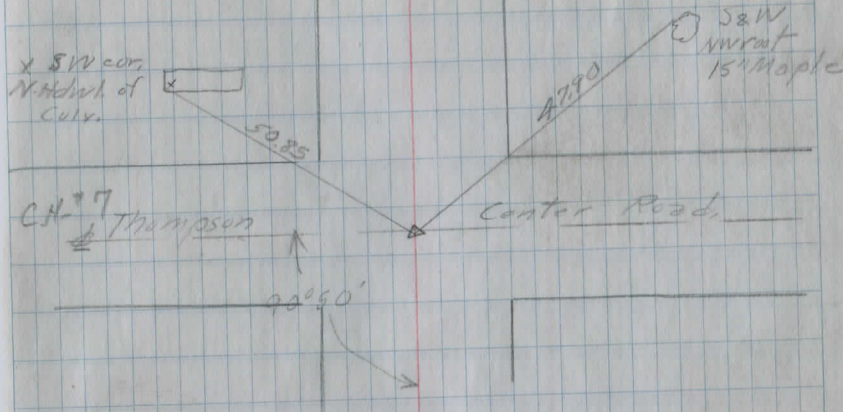
84

83

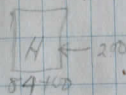
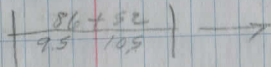
82

81

80



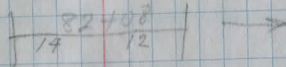
3/2 x 2  
 Stone Box Culv.  
 Fair condition



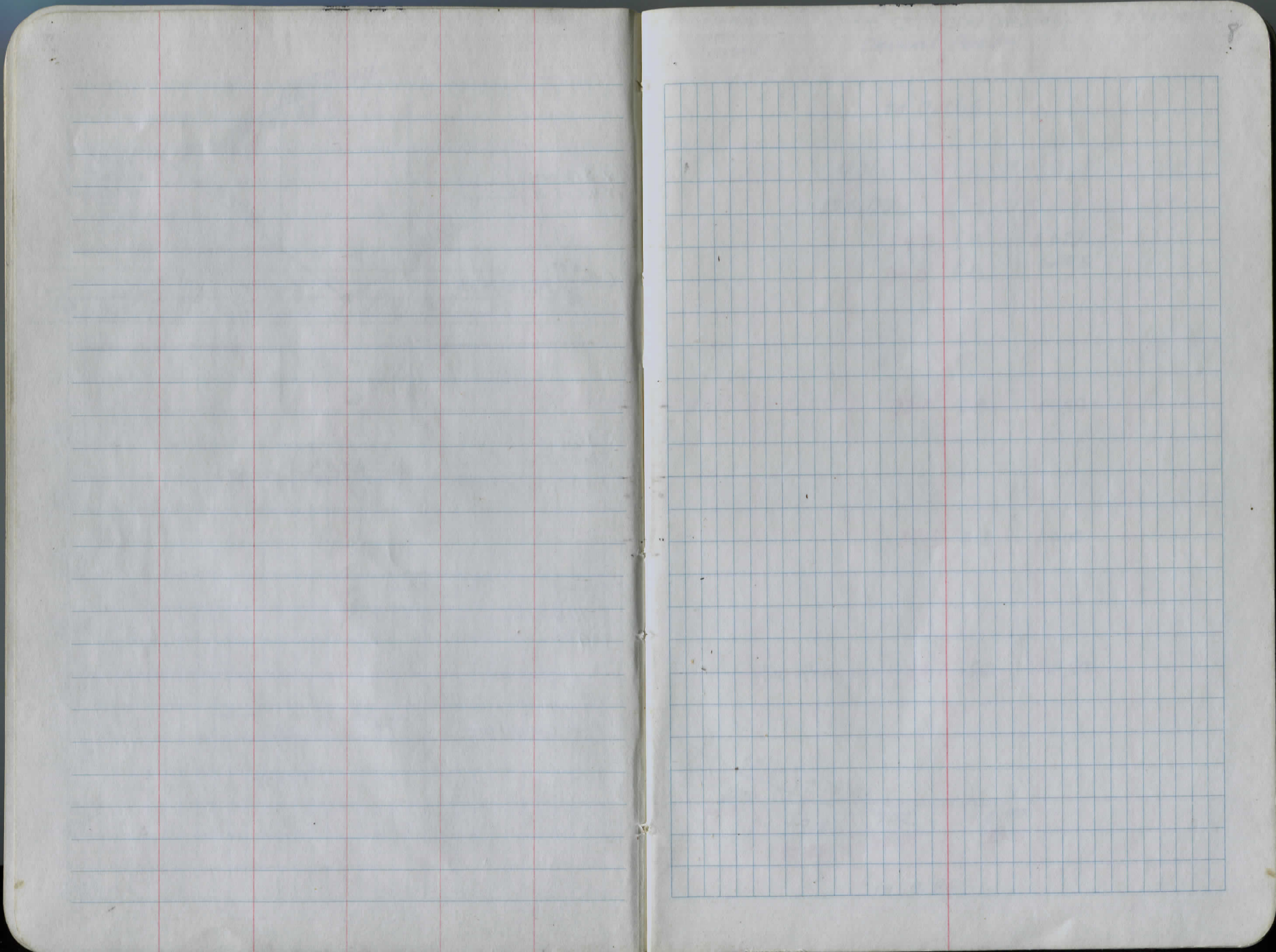
Drive 84+00

N 2° 04' 57" E

3 x 2  
 Stone Box Culv.  
 Fair condition



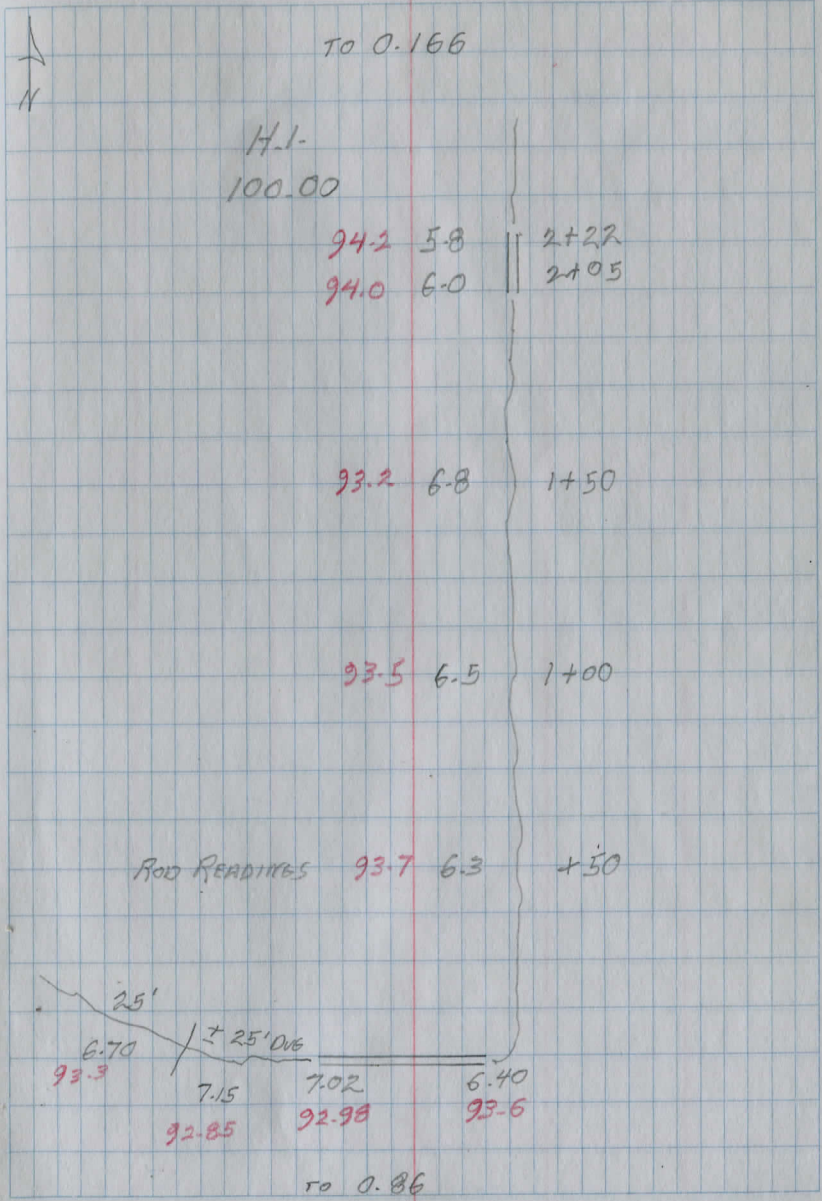
81+28 x x



R.E. HERSHBERGER  
G.L. KOVACH  
M.A. FERGUSON

T.R. 53 J CLAY (WEBSTER)  
DRAINAGE PROBLEM

9 NOVEMBER 1984  
9



A grid of 20 columns and 20 rows, drawn with blue lines on a white notebook page. The grid is rectangular and occupies most of the page's width and height. A vertical red margin line is visible to the left of the grid.

T.H. 56

	+	H.L.	-	
BM	0.40	1282.07		128167
	11.32	1280.47	12.92	1269.15
0+00			10.2	1270.27
BM #1			11.13	1269.34
Colv. 0+24				
1			9.1	1271.37
2			3.8	1276.67
	10.60	1290.60	0.47	1280.
3			9.8	1280.80
3+50		Rock	9.0	1281.60
4			8.5	1282.10
4+30		Rock	7.7	1282.90
4+50			6.8	1283.80
5			6.0	1284.60
6			3.6	1287.00
7			2.6	1288.00
8			0.8	1289.80
	9.63	1300.15	0.08	1290.52
9			8.1	1292.05
9+20		Rock	7.1	1293.05
10			6.1	1294.05
11			5.0	1295.16
11+20			4.3	1295.85
BM #2			3.78	1296.37

3/18/38

11

Road.

BM #1 Tillotsons Cor. E. Rd. Sta 9+60

Spike N. root 24" Maple 25' South of  $\frac{1}{4}$  and 500'  
West of Sta 0+00 Under Ledge Rd.

X out NW Cor. W Headwall Culvert Sta 0+24

$$\begin{array}{r} 70 \\ 12.8 \\ \hline \end{array}$$

$$\begin{array}{r} 1.0 \\ 11.8 \\ \hline \end{array}$$

$$\begin{array}{r} \text{Rock} \\ 2.2 \\ \hline \end{array}$$
Spike S. Root 15" Maple 25' Lt  $\frac{1}{4}$  Sta 11+50

130015

12			Root 3.0	1297.16
13			Root 4.0	1296.15
13 + 40			Root 5.0	1295.16
	1.52	1291.68	9.99	1292.16
14			6.5	1290.18
15			3.7	1287.98
16			4.8	1286.88
16 + 93			5.2	1286.5
17			5.3	1286.38
18			5.3	1286.38
19	3.12	1289.47	5.33	1286.35
19 + 60				
20			3.5	1285.97
21			4.1	1285.37
BM#3			4.21	1285.26
22			5.8	1283.67
22 + 10			Root 5.8	1283.67
22 + 65	0.35	1276.97	12.85	1276.62
23			4.8	1272.17
23 + 50			9.6	1267.37
24			12.3	1264.67
	0.48	1265.09	12.36	1264.61
25			4.1	1260.99
26			8.1	1256.99
27			11.9	1253.19

$\frac{PI}{7.9}$	$\frac{PI}{6.9}$
------------------	------------------

$\frac{10}{3.2} R$
$\frac{10}{8.6} R$

Spike W. root 36 Maple 28' L + Sta 21 + 29

		1265.09		
	0.07	1252.85	12.31	1252.78
28			2.0	1250.85
29			5.5	1247.35
30			11.8	1241.05
	2.41	1244.03	11.23	1241.62
31			5.2	1238.8
BM#4			3.50	1240.53
32			3.6	1240.43
33			3.0	1241.03
34			4.1	1239.93
34+77			4.8	1239.23
	0.29	1240.23	4.09	1239.94
35			1.6	1238.63
36			3.1	1237.13
37			4.3	1235.93
38			5.4	1234.83
39			6.7	1233.53
40			8.2	1232.03
	2.25	1234.14	8.34	1231.89
41			3.3	1230.69
42			4.4	1229.74
43			5.9	1228.24
44			11.3	1222.84
BM#5	0.47	1223.82	10.79	1223.35

	$\frac{50}{73}$	$\frac{Fl}{9.6}$	$\frac{Fl}{9.8}$	$\frac{50}{14.5}$
Spike E. root 10' Maple 18' Rt. ± Sta 30+30				
	1240.53			
	10.23			
	<u>1250.76</u>	H.I.		24 <sup>2</sup> Right, Sta. 28+35
	0.18			New B.M., ref. spike, W. side 15' Apple
El.	1250.58			
	$\frac{Fl}{6.0}$	$\frac{Fl}{6.1}$	$\frac{50}{7.9}$	

Spike W. root 18' Maple 20' Rt ± Sta 44+35

1223.82

44+84			4.5	1219.32
45			4.2	1219.62
46			6.2	1217.62
46+85			8.0	1215.82
47			8.1	1215.72
48			11.0	1212.82
	0.92	1215.62	9.12	1214.70
49			4.3	1211.32
49+86			4.5	1211.12
50			7.2	1208.42
51			9.5	1206.12
BM#6	0.20	1208.52	7.30	1208.52
52			5.7	1202.82
53			8.8	1199.72
54			11.7	1196.82
	1.18	1197.86	11.84	1196.68
54+74			1.9	1195.96
55			2.0	1195.86
56			3.0	1194.86
57			7.9	1189.96
57+87			11.1	1186.76
58			11.1	1186.76
58+70			10.5	1187.36
59	0.77	1187.03	11.60	1186.26
60			3.7	1183.33

$$\frac{35}{12.5} \quad \frac{FL}{12.0} \quad \frac{FL}{18.0} \quad \frac{30}{20.0}$$

$$- \quad \frac{FL}{11.2} \quad \frac{FL}{11.0} \quad \frac{30}{13.3}$$

246

$$\frac{35}{43} \quad \frac{FL}{69} \quad \frac{FL}{8.3} \quad \frac{30}{10.8}$$

2 Vert. spikes Erect 48" Maple 25' LT & Sta 51+40

$$- \quad \frac{FL}{7.4} \quad \frac{FL}{7.6} \quad \frac{30}{10.0}$$

1187.03

61		72	1179.83
62		8.4	1178.63
62+65		8.5	1178.53
62+80		9.0	1178.03
63		9.4	1177.63
	1.00	1176.91	11.12 1175.91
64		0.8	1176.11
64+60		1.2	1175.71
65		5.1	1171.81
BM#7		6.05	1170.86
66		10.6	1166.21
66+73		11.3	1165.61
67		11.1	1165.81
68	2.43	1172.13	7.21 1169.70
68+45		0.6	1171.53
69		2.0	1170.13
70		4.6	1167.53
71		6.4	1165.73
71+51		6.8	1165.83
72		6.9	1165.73
73		6.1	1166.03
	1.95	1166.83	6.45 1165.68
74		2.0	1164.83
BM#8		10.08	1166.91
75		3.0	1163.83

—	Fl	Fl	25
	10.9	12.4	13.7

Spike W.root 18" Maple 25' Rt of & Sta 65+60

30	Fl	Fl	60
13.4	15.3	16.0	17.2

—	Fl	Fl	50
	8.3	9.3	11.4

Spike NE root 24" Maple 28' Lt & Sta 74+75

116683

76		5.8	1161.03	
76+68		6.8	1160.03	
77		6.6	1160.23	
78		4.7	1162.13	
78+30		4.3	1162.53	
79		5.4	1161.43	
	1.34	1162.42	5.75	1161.08
80		3.9	1158.52	
81		11.8	1150.62	
	2.64	1152.12	12.94	1149.48
82		4.6	1147.52	
82+08		4.7	1147.42	
83		3.0	1149.12	
	6.71	1156.22	2.61	1149.51
84		0.6	1156.62	
85		5.1	1151.12	
86		10.8	1145.42	
86+52		11.2	1145.02	
87		9.7	1146.52	
87+49		5.7	1150.52	
87+40		5.9	1150.32	
B11#9		5.69	1150.53	1150.98 <sup>Rec.</sup>

16

25	Fl	Fl	30
80	10.1	11.4	11.9

SWAMP	Fl	Fl	40	100
10.6	11.3	11.7	10.9	11.0

Fl	H	H	Fl	25	75	150
10.2	11.1	11.1	15.6	15.7	15.9	16.8

100	100
5.6	3.2

Cross cut SW Cor. North Headwall Culvert 50' Lt Sta 87+60

Culvert at Sta

58

1.6

11884

1186.8

$\frac{25}{7.2}$

$\frac{FL}{10.0}$

$\frac{FL}{11.7}$

$\frac{30}{13.0}$



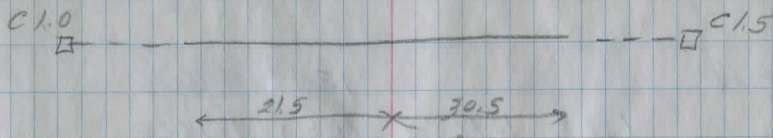
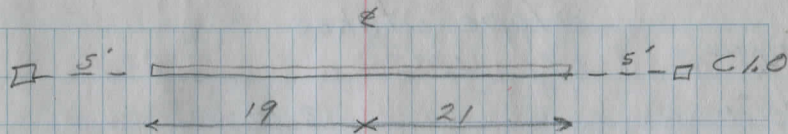
### Culvert at 54+74

BM#6	105.20		
± Road	5.2		
Flow L	10.70		
Stake L	10.42	9.42	C1.0
Flow R	13.00		
Stake R	13.28	12.28	C1.0

### Culvert at 57+90

± Road	1.5		
Flow R	12.5		
Stake P	12.80	11.30	C1.5
Flow L	9.6		
Stake L	9.30	8.30	C1.0

50 | 300  
 .6 pm 10



# Slope Stakes

BMI # 3	3.99	128925	1285.26
20 + 50		3.79	1285.46
21		4.94	128431
21 + 50		6.79	1282.46
22		9.29	1279.96
22 + 50		12.49	1276.76
	1.22	1278.84	10.63 1278.62
23		6.94	1272.90

LT	E	RT
$\frac{F 0.5}{19.0}$		$\frac{C 2.0}{21.8}$
$\frac{C 0.8}{20.4}$		$\frac{C 3.0}{23.3}$
$\frac{C 2.9}{23.6}$		$\frac{C 4.3}{25.7}$
$\frac{C 4.2}{26.0}$		$\frac{C 3.1}{24.2}$
$\frac{C 6.6}{28.8}$	$\frac{4}{C 1.5}$	$\frac{C 0.8}{20.3}$
$\frac{C 6.9}{28.0}$	$\frac{6}{F 1.1}$	$\frac{F 6.0}{22.0}$

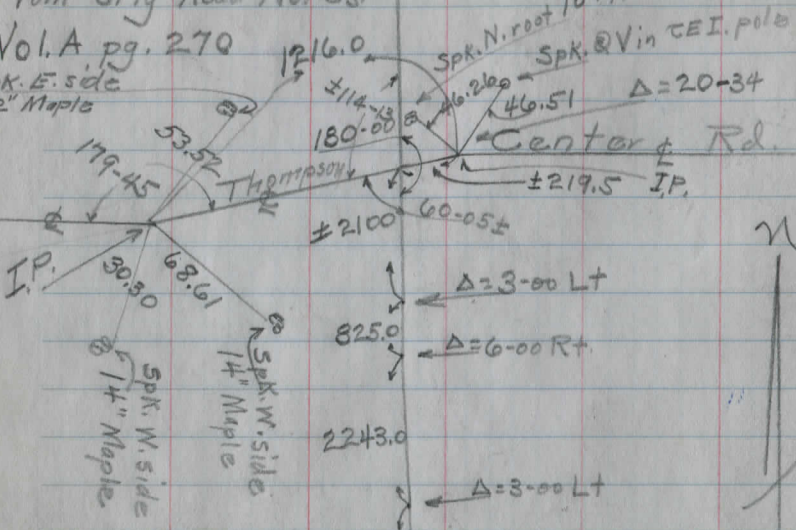
Webster (Wilber) Road (Co. Hwy) #53

Thompson Twp, Sec. K  
CLAY STREET

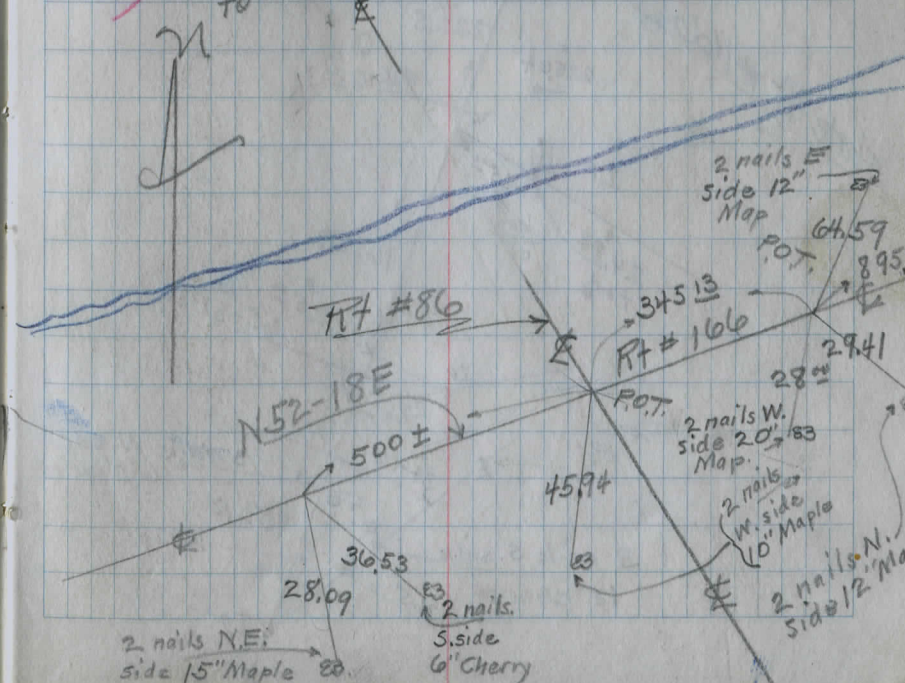
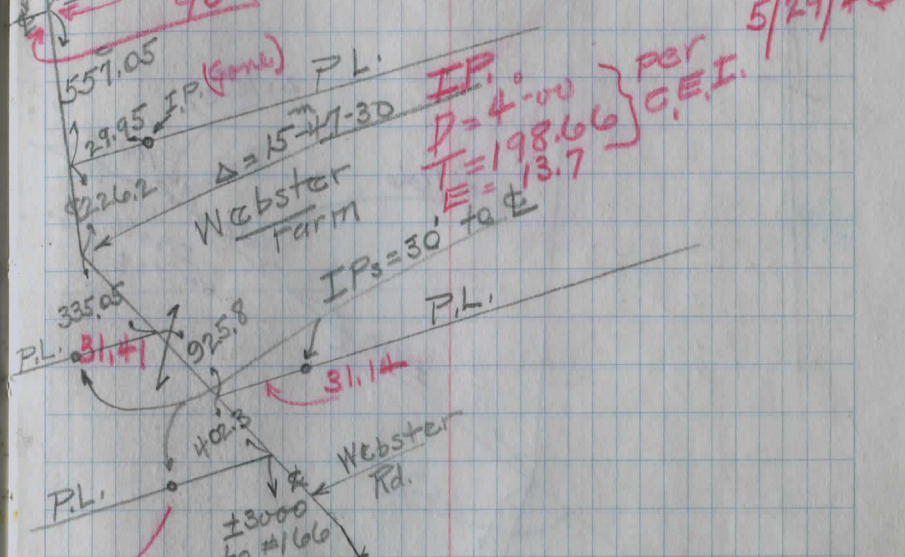
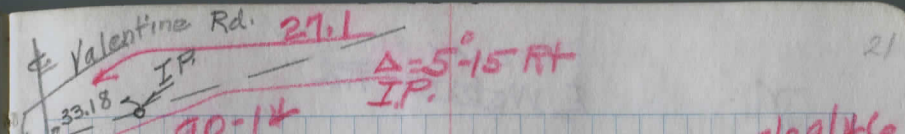
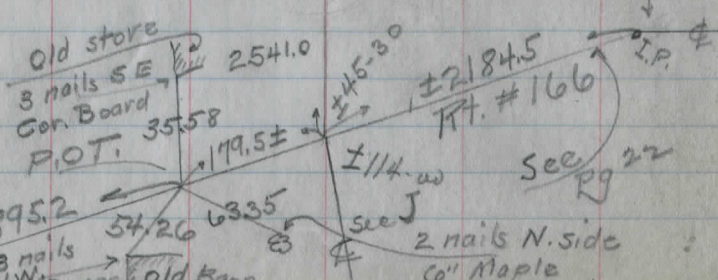
From Orig Road Notes.

Vol. A pg. 270

Spk. E. side  
12" Maple

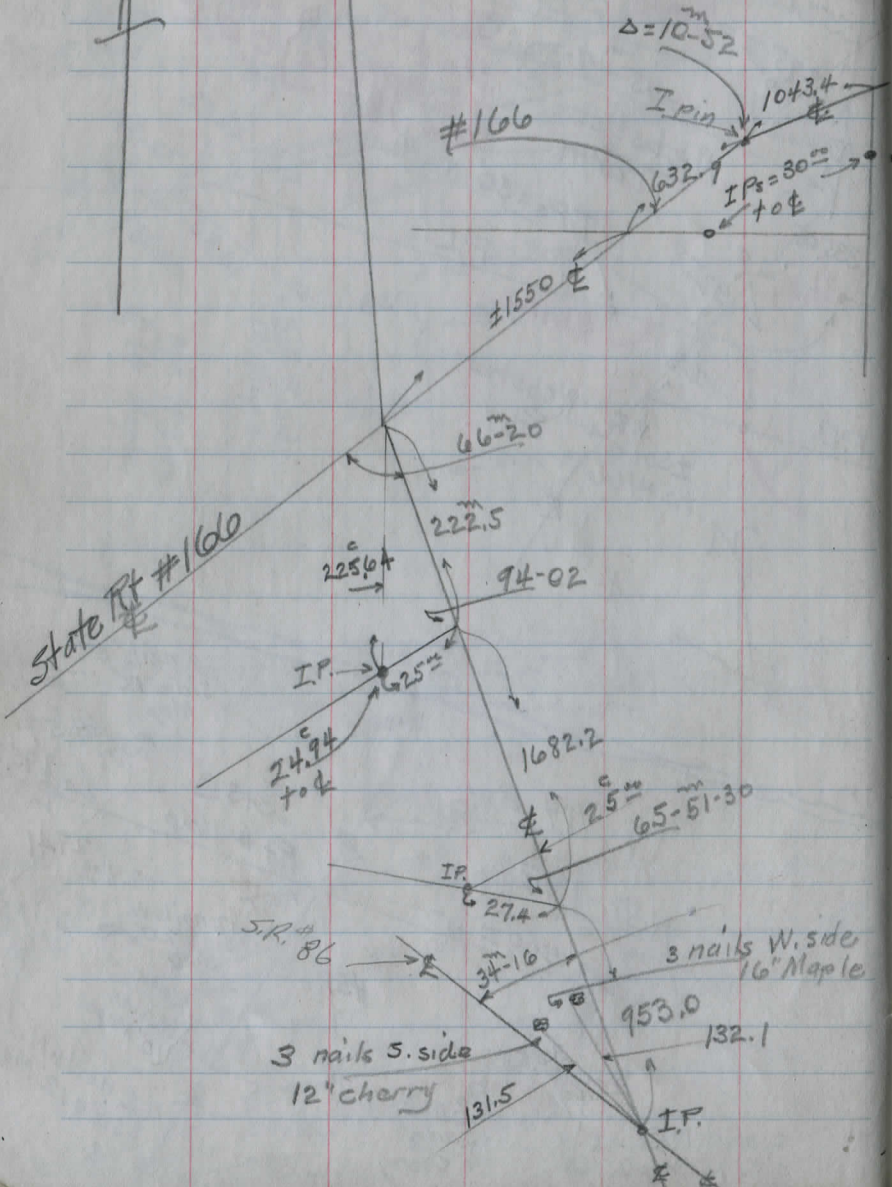
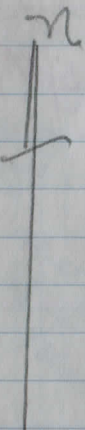


See opposite page



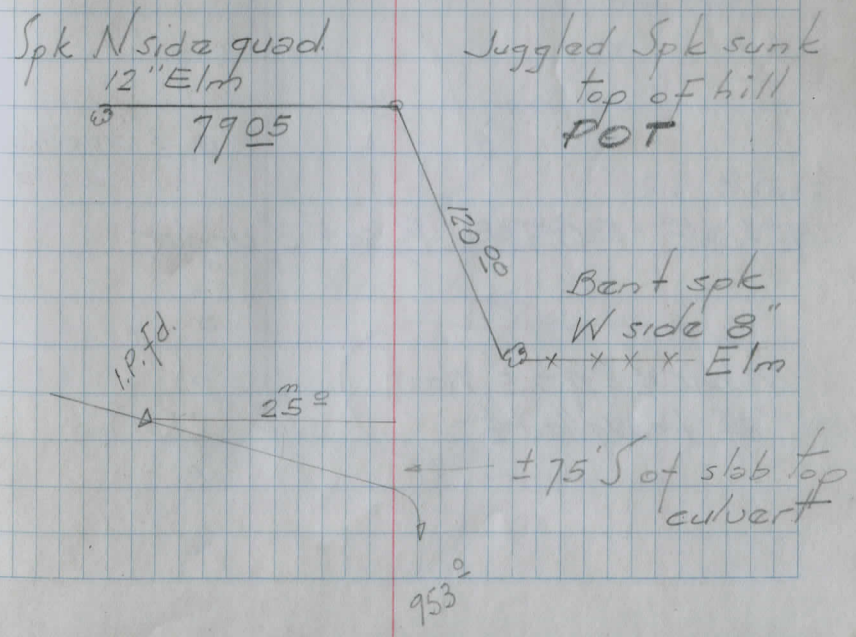
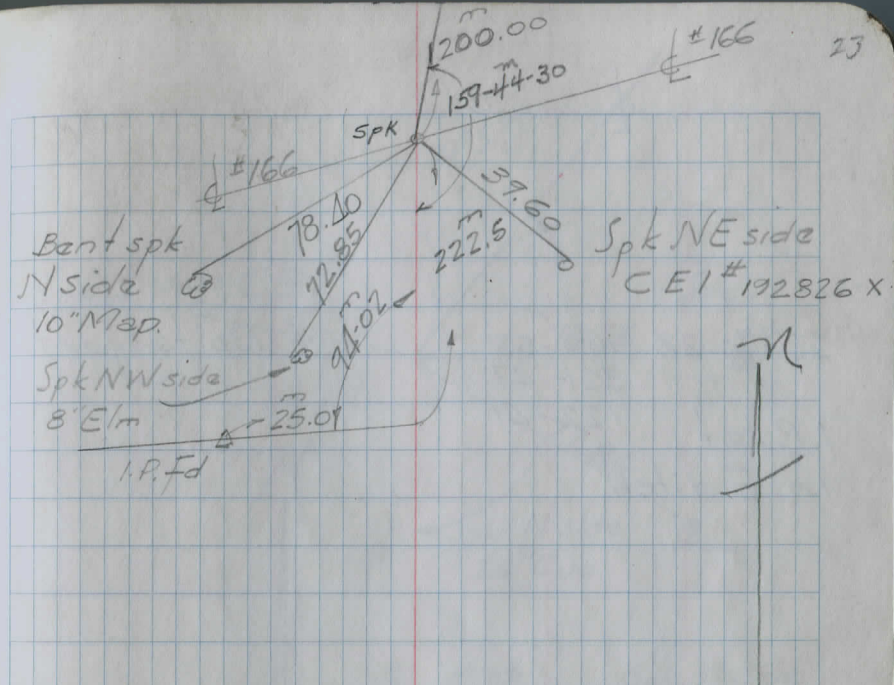
CLAY ST. T. 4.53

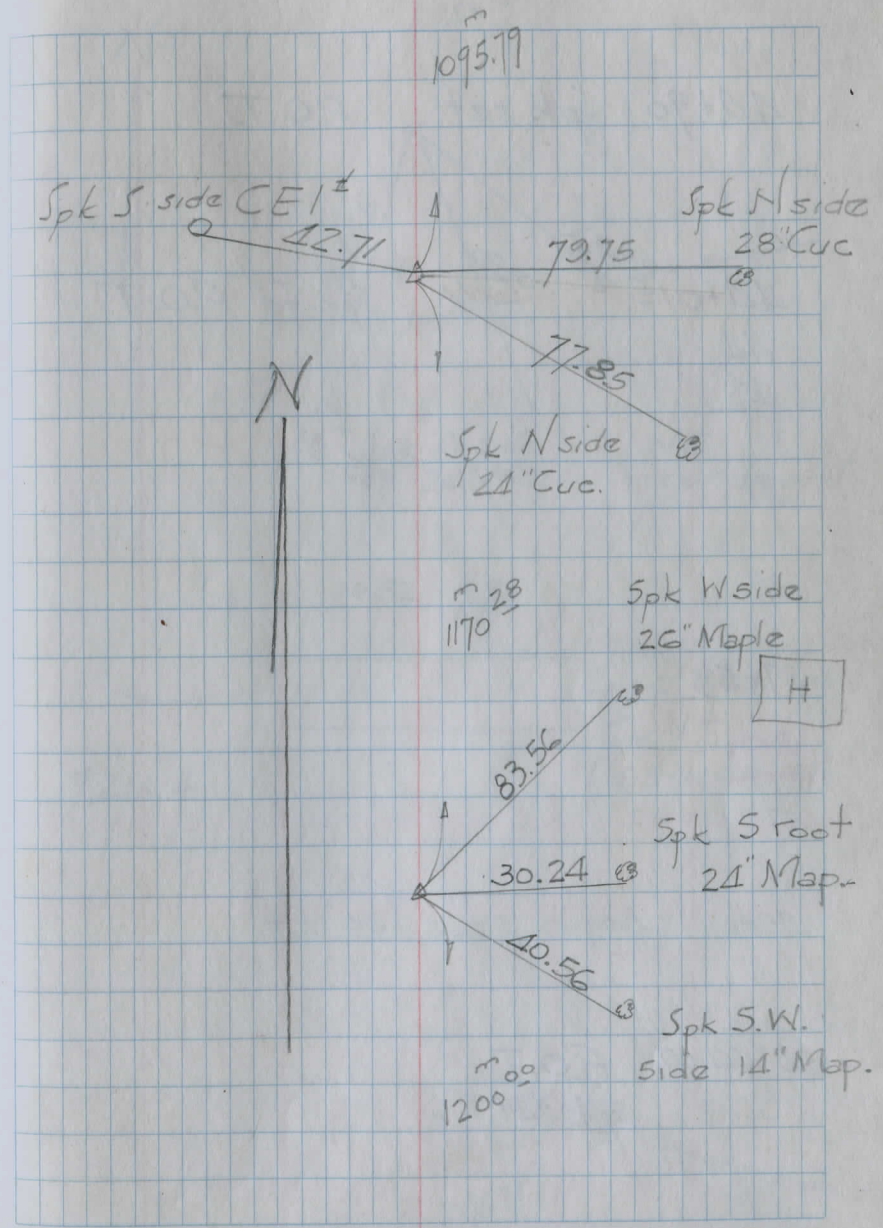
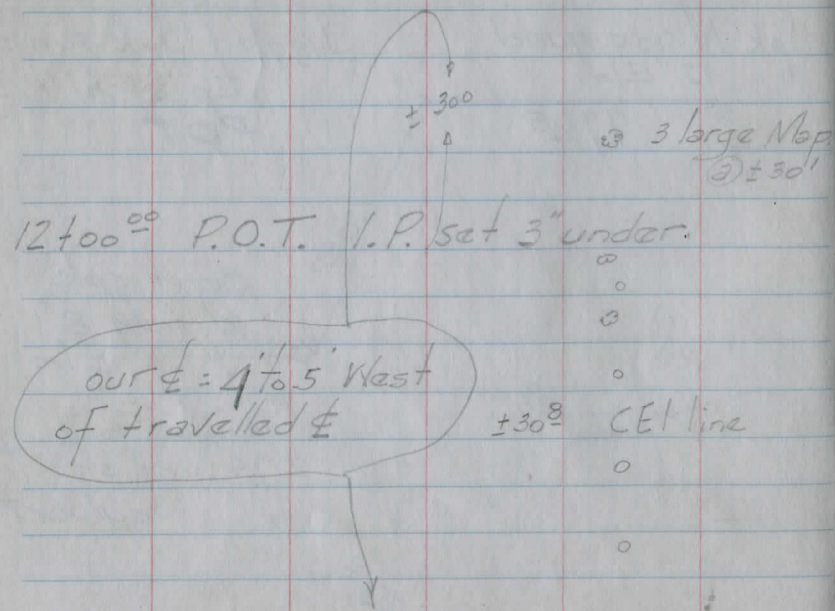
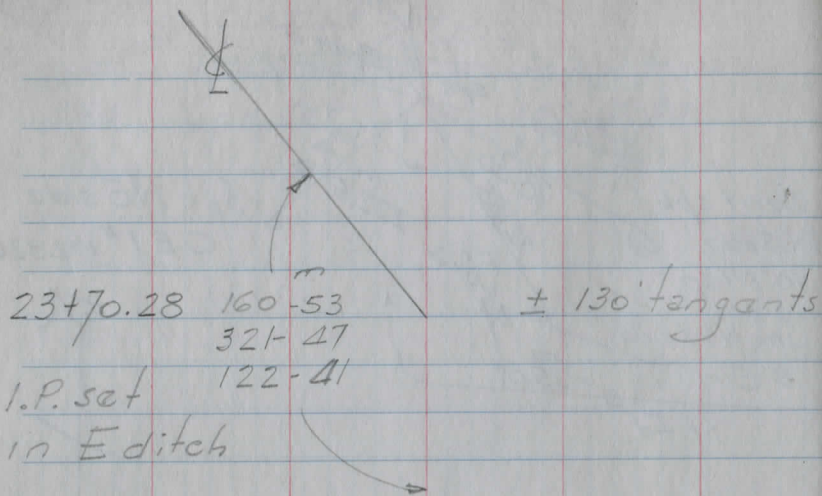
Webster Rd



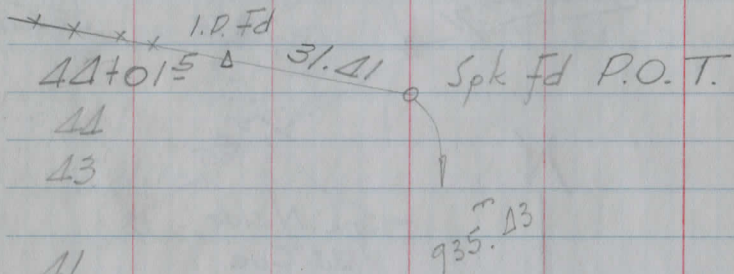
10-14-06  
Tom Maynard  
Randles

CLAY ST. TH. # 53 J ±  
WEBSTER RD  
Spk set 159-44-30  
319-29





44+90 Spk set P.O.T.



44

43

41

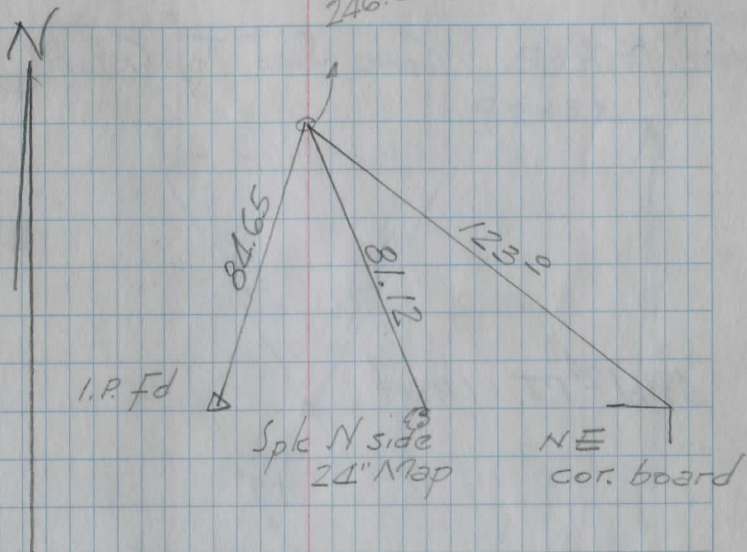
39

37+58

37

35 to begin stks (30' Rf)

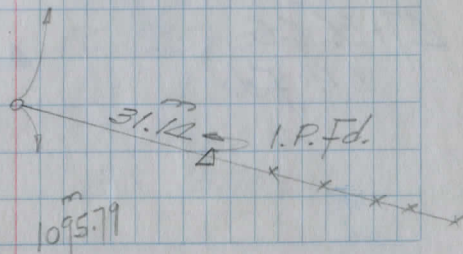
31+66.07 P.O.T.  
Spk set



10.52 9.85

9.2 x 4'

Conc Slab Top  
Culot ~~10.71~~  
(53-K-10.79)



49+91

Conc. Slab Top Culvert

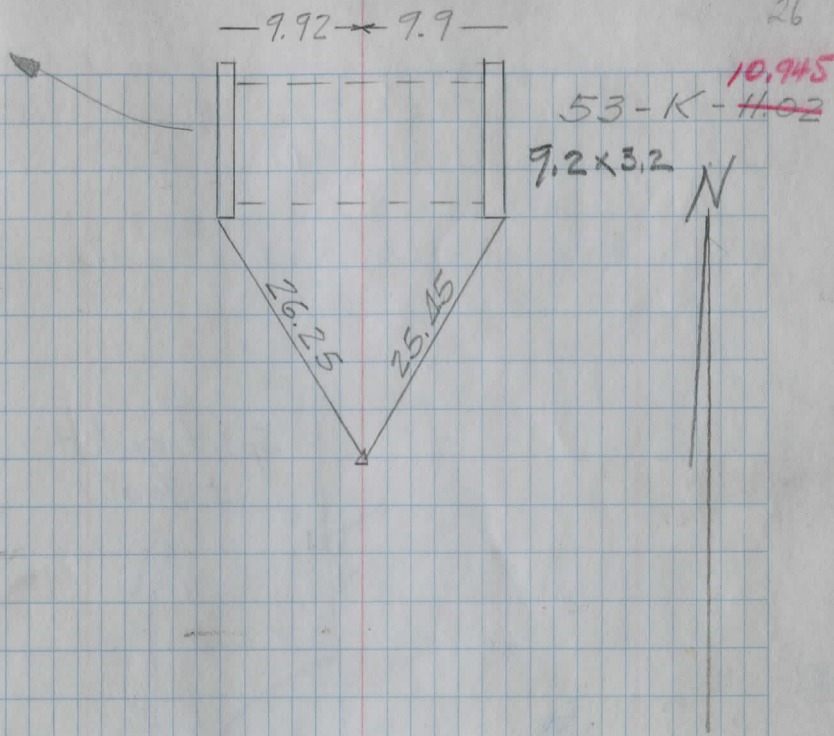
49+61<sup>04</sup> P.T. I.P. set



± 9°

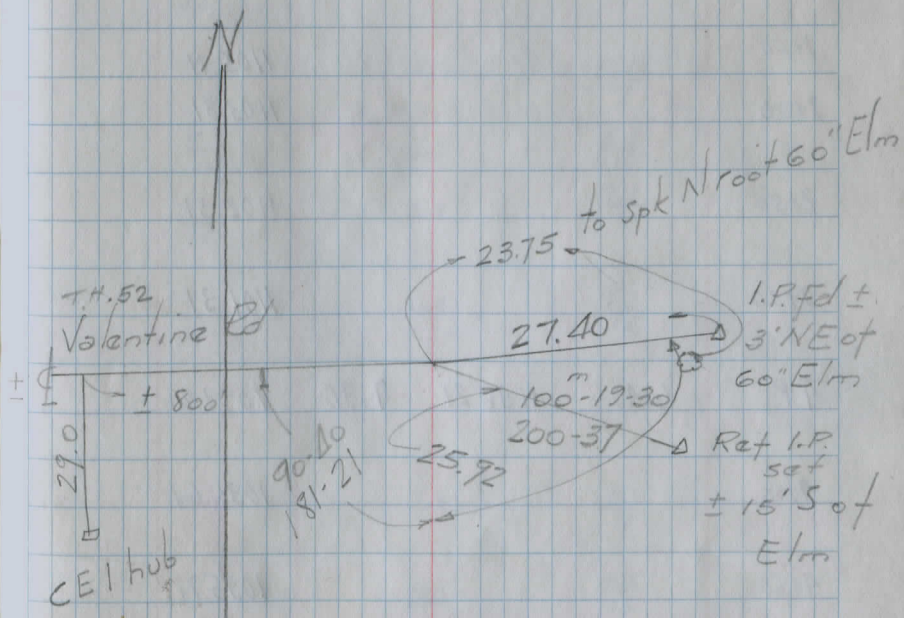
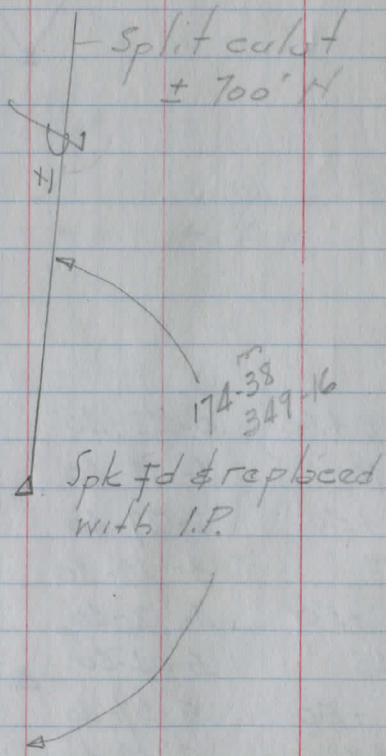
x x | x PL.  
"No find I.P."

47+36.65  
I.P. Fd.



45+50	0-12-40	Δ = 15-48-30 RT.
46	1-34-40	D = 3°-30'
+50	2-27-40	R = 1637.022
47	3-19-40	P.I. = 47+36.65
+50	4-12-40	T = 2 27.28
48	5-04-40	PC = 45+09.37
+50	5-57-40	L = 4 51.67
49	6-49-40	P.T. = 49+61.04
+61 <sup>04</sup>	7-54	E = 15.70

55+16.50



8-19-56 Clear-Warm 70°

Patterson  
Canfield  
Raffie

Sta.	+	HI	-	Elev
BM #11	2.59	1114.29		1111.70
T.P.	3.79	1114.01	4.07	10.22

0+0 Intersection Clayst. & Thompson Rd. Ditch's  
1108.61

0+50  
T.P. 2.70 1107.71 9.00 1105.01  
1107.21

1+00 1106.31

1+50 1105.11

2+00 1103.81

2+50 1102.31

3+00 1101.31

T.P. 6.40 1106.21 7.90 1099.81

4+00 1096.61

4+50 1095.71

5+00 1095.01

Levels Clayst, North of Thompson Rd. 28

BM #11 Vert. Spk. S. Root 24" Maple 32' Lt. Sta 67+90  
(Thompson Rd. see Field Bk. 121 pg. 15)

W. Ditch	E	E. Ditch
$\frac{6.9}{15}$	6.9	$\frac{6.5}{30}$

$\frac{8.1}{15}$	6.8	$\frac{7.7}{15}$
------------------	-----	------------------

$\frac{2.6}{15}$	1.4	$\frac{2.7}{15}$
------------------	-----	------------------

$\frac{3.9}{15}$	2.6	$\frac{4.1}{15}$
------------------	-----	------------------

$\frac{5.7}{15}$	3.9	$\frac{5.8}{15}$
------------------	-----	------------------

$\frac{6.7}{15}$	5.4	$\frac{7.1}{15}$
------------------	-----	------------------

$\frac{7.5}{15}$	6.4	$\frac{8.3}{15}$
------------------	-----	------------------

10.6	9.6	$\frac{11.1}{15}$
------	-----	-------------------

11.2	10.5	$\frac{11.5}{15}$
------	------	-------------------

12.0	11.2	12.2
------	------	------

	+	HI	-	Elev
		1106.21		
5+50				1094.61
				1098.6
0+00				1098.1
				1097.6
1+00				1095.5
2+00				1095.0
3+00				
TP	11.30	1114.31	3.20	1103.01
TP	4.70	1114.71	4.30	1110.01
BM #11			2.94	1111.77

W. Ditch		E. Ditch
12.6	11.6	12.8

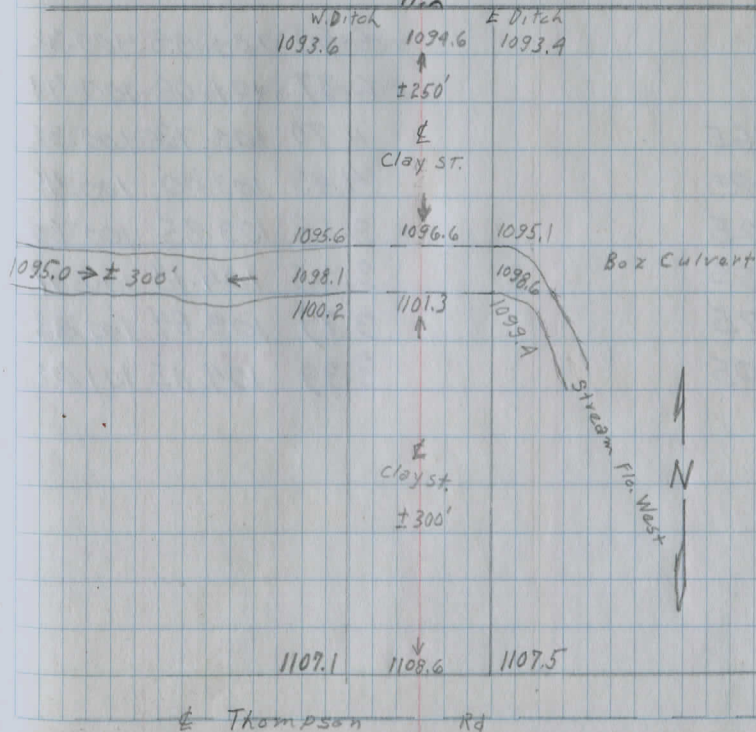
Ditch running W across Clay St.  
 ± 300' N. of + Clay St. - Thompson Rd.

INlet	7.6
Outlet	8.1

8.6

10.7

11.2



STA.	B.S.	H.I.	F.S.	ELEV.	$\frac{1}{2}\%$ F.G.R.	CUT
0+00	7.43	107.43		100.00		
0+50			7.00	100.43	100.25	0.18
1+00			5.70	101.73	100.50	1.23
1+50			5.01	102.42	100.75	1.67
1+55			5.01	102.42	100.76	1.66
1+75			4.99	102.44	100.88	1.56
2+00			4.74	102.69	101.00	1.69
2+50			4.45	102.98	101.25	1.73
3+00			3.99	103.44	101.00	1.94
			6.50	100.93	100.32	0.61
			6.37	101.06	100.45	0.61
0+65			4.70	102.73	100.32	2.41
0+85			4.43	103.00	100.45	2.55
1+25			3.58	103.85	100.68	3.17
1+55			3.25	104.18	100.76	3.42
1+75			3.79	103.64	100.88	3.16
2+05			3.39	104.05	101.02	3.02

R.E.H.  
G.L.K.  
M.A.F.

SW DITCH ON TR 53 J CLAY  
AT 0.166 FOLK CREEK RD. INT.

28 OCTOBER 1983  
50°F. FAIR  
WIND SW 20 MPH

W INV. CULV. X CLAY S OF 166

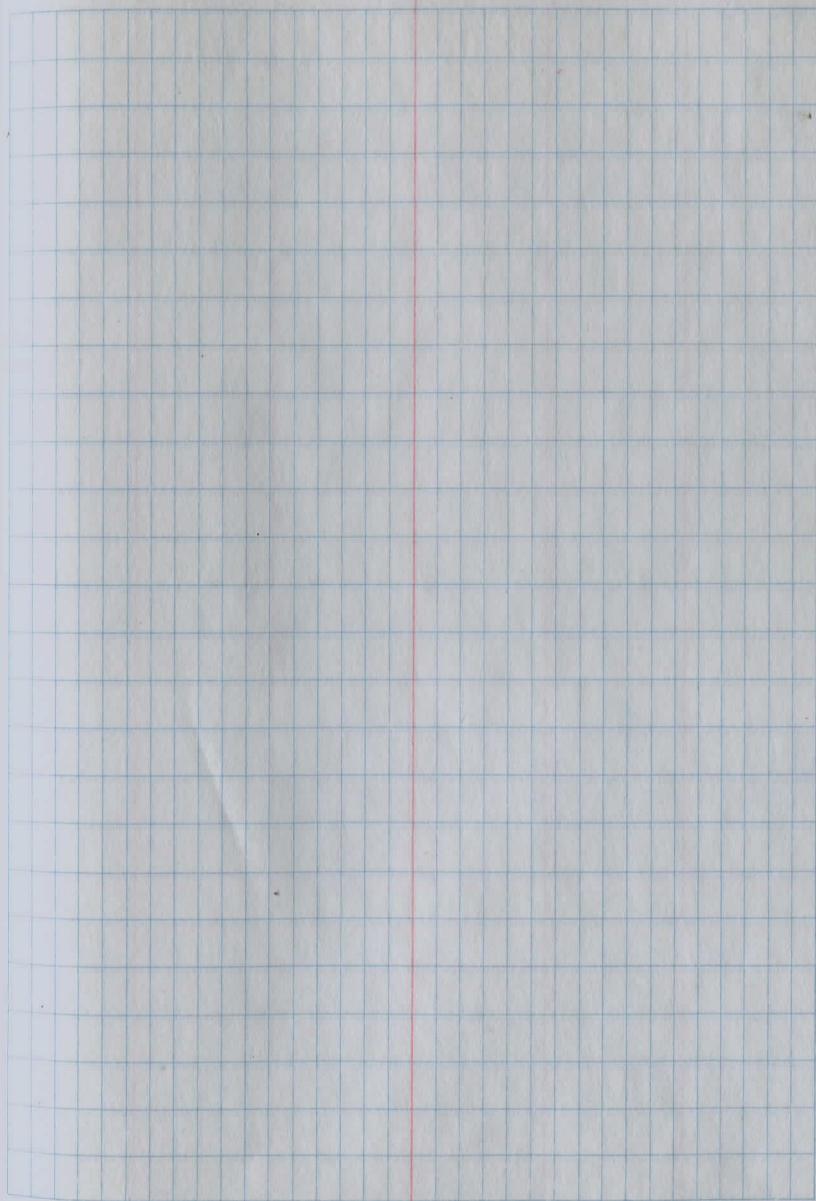
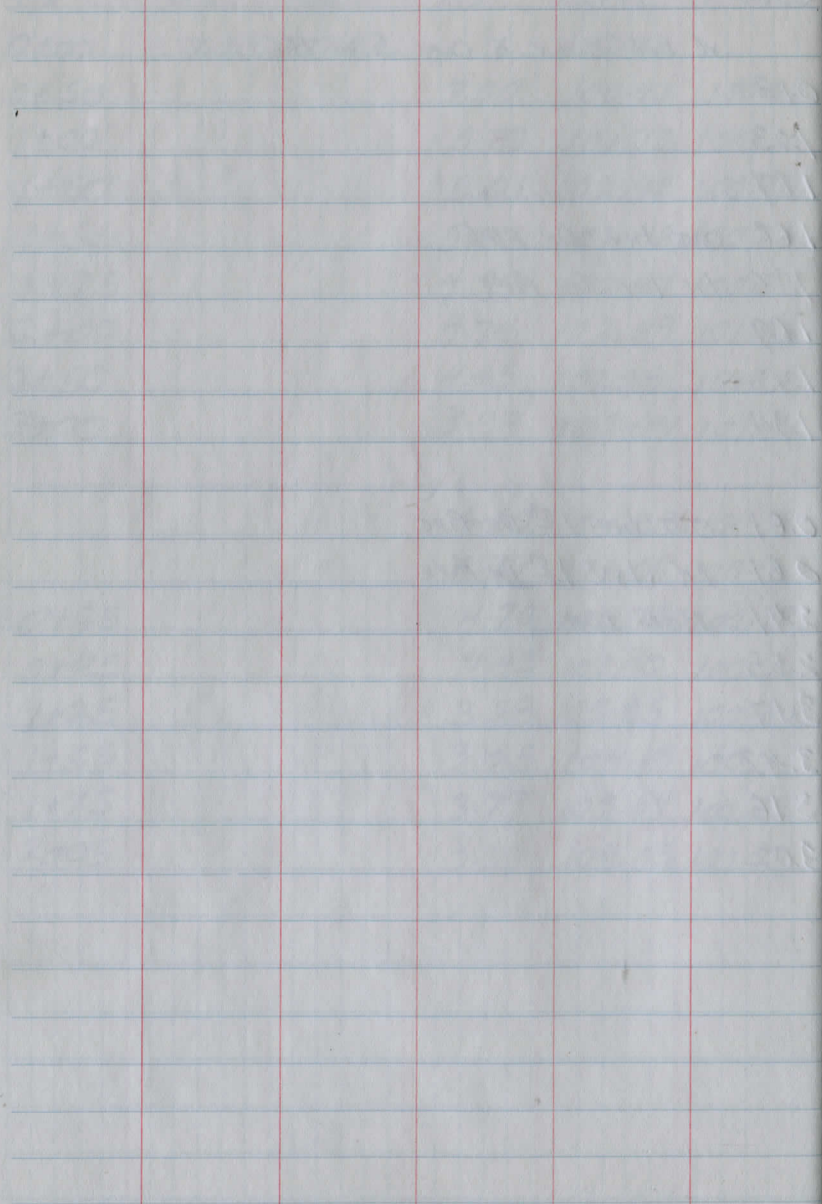
OUT INV. DR. PIPE

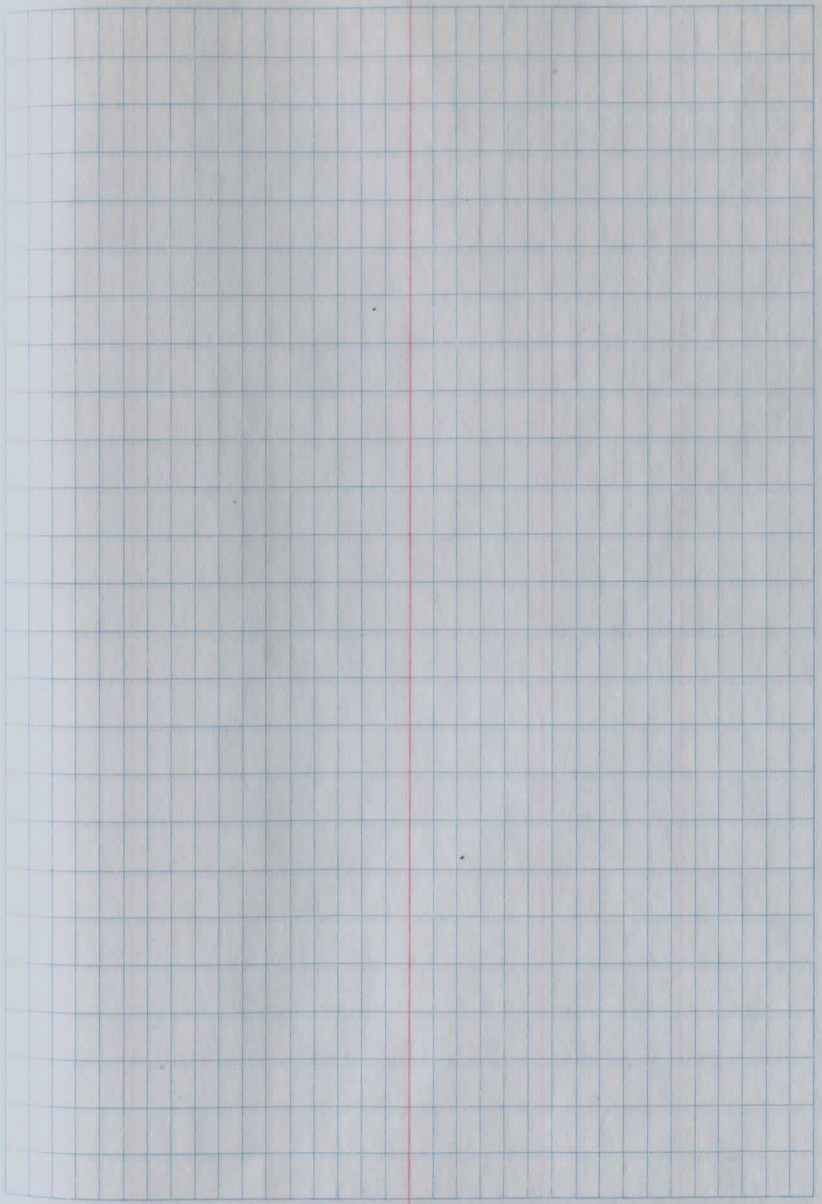
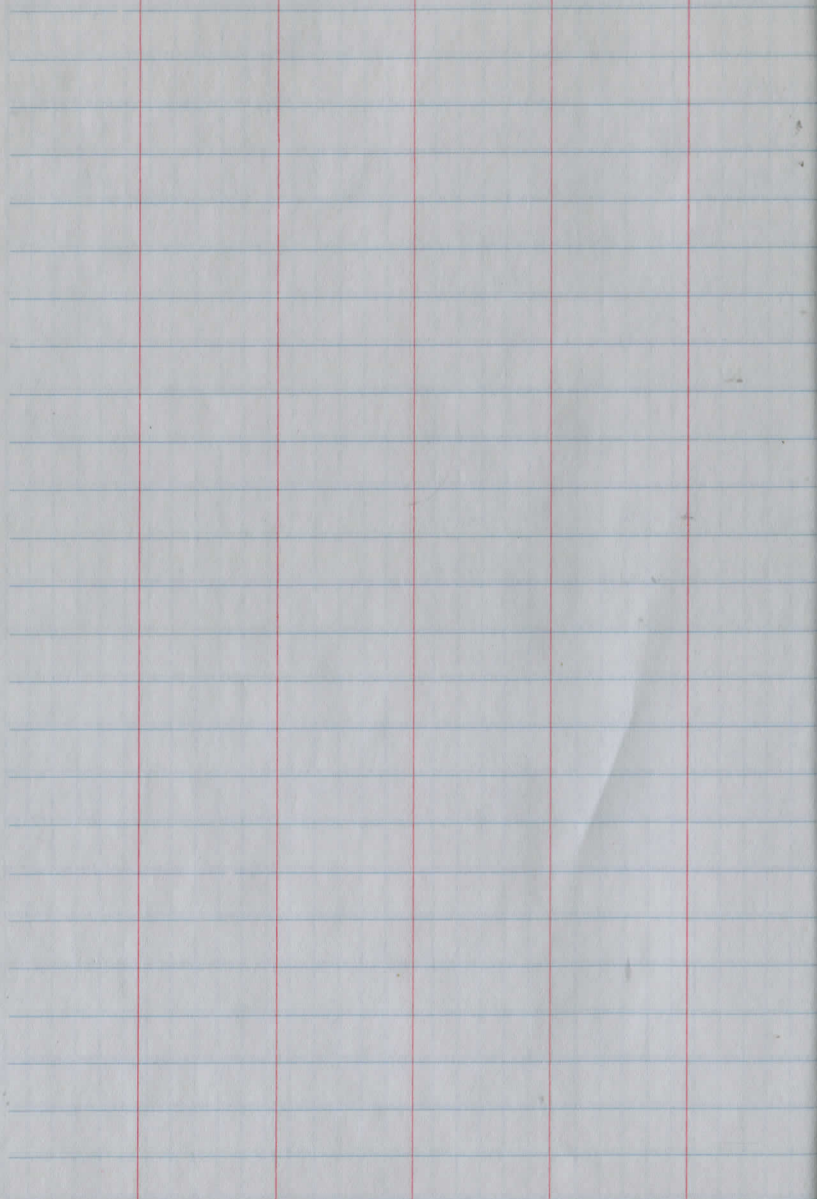
1/4 INV. DR. PIPE

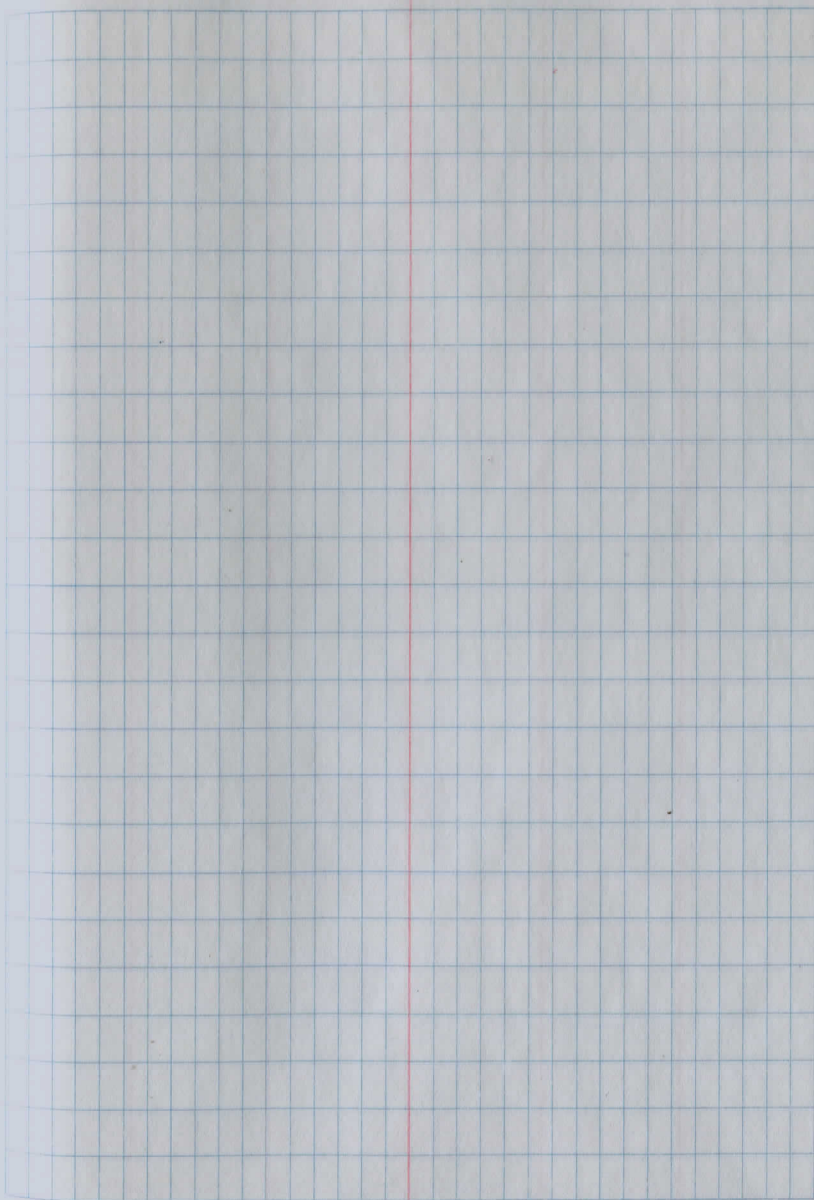
OUT INV. 1<sup>st</sup> DR. PIPE

1/4 INV. 1<sup>st</sup> DR. PIPE

ROD TOP

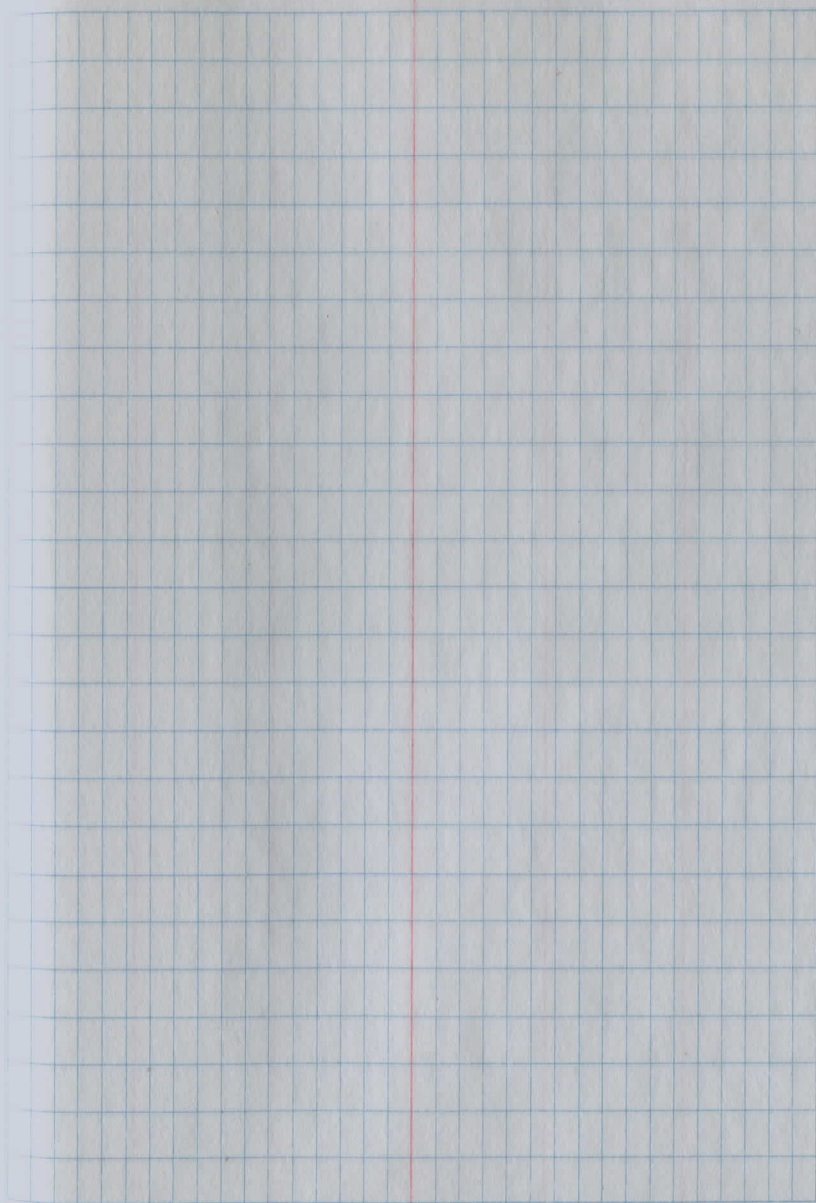


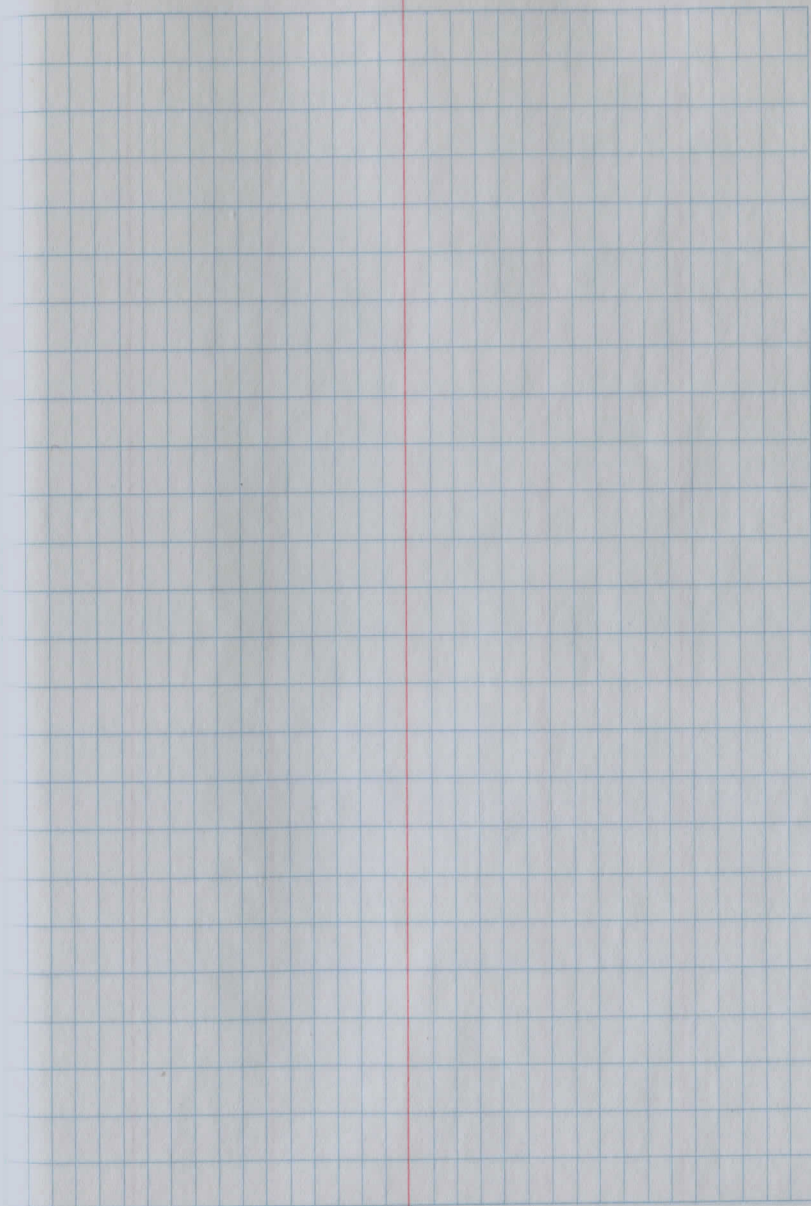
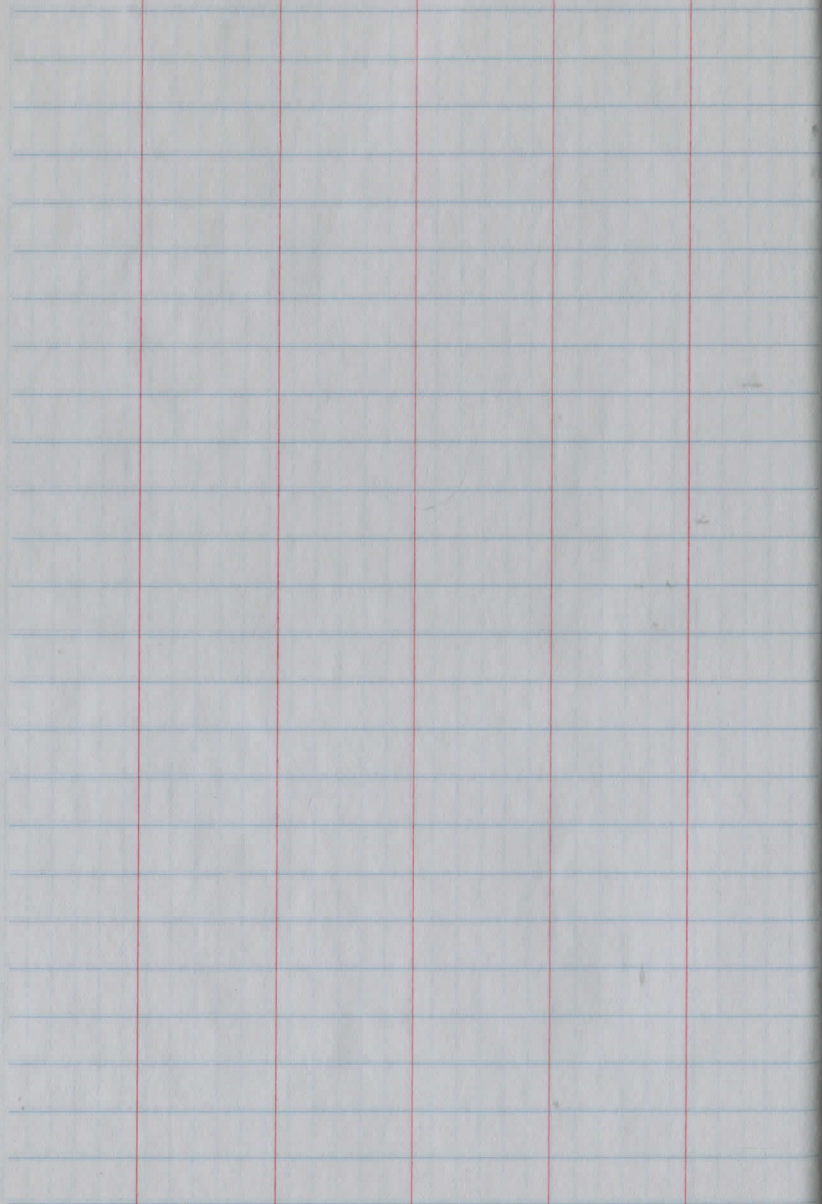


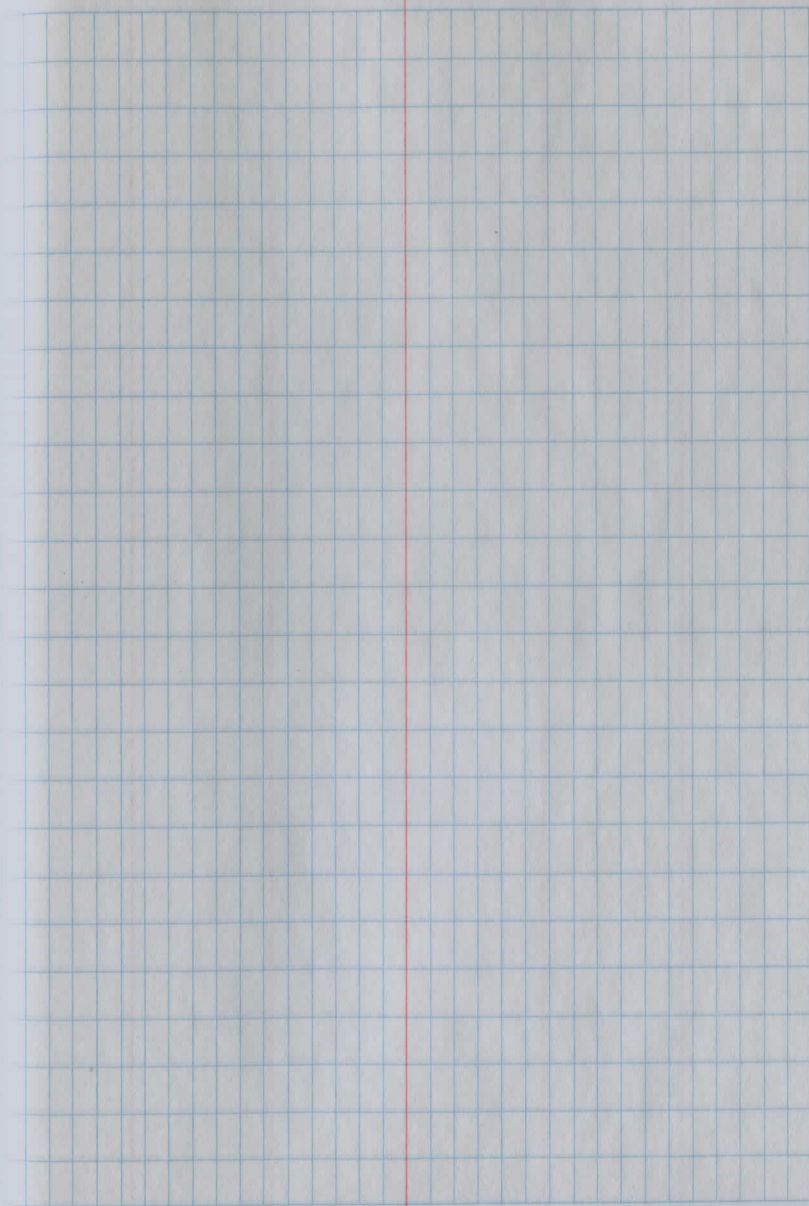
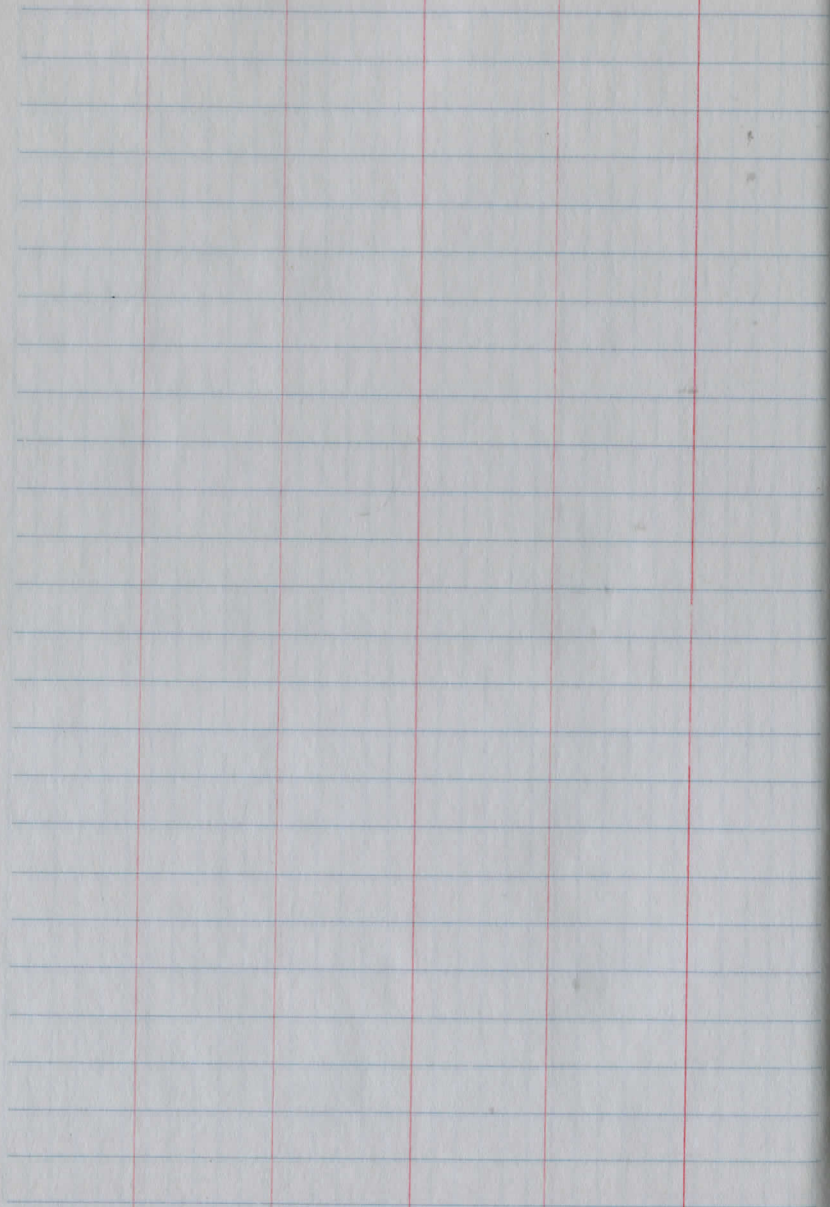


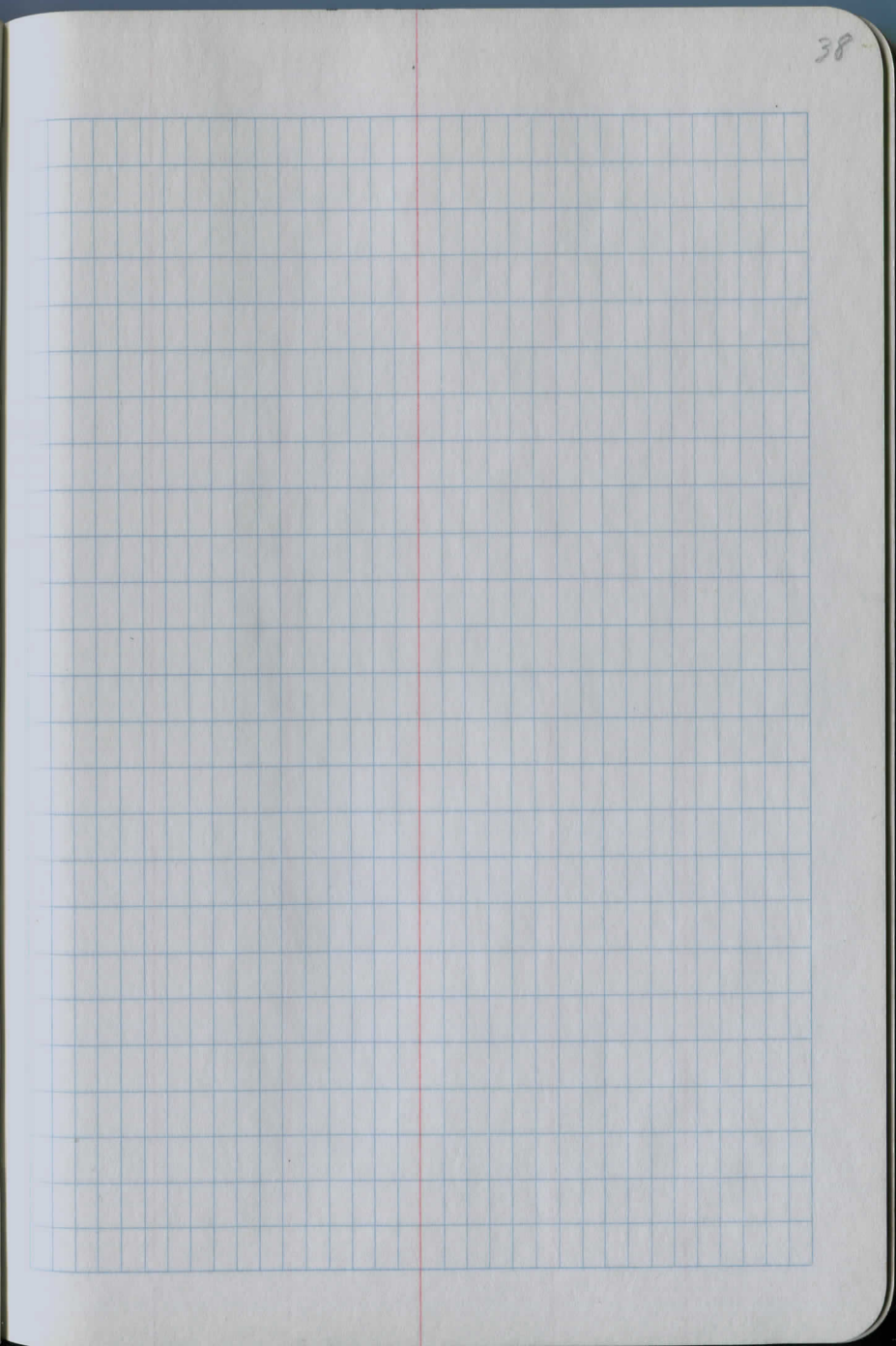
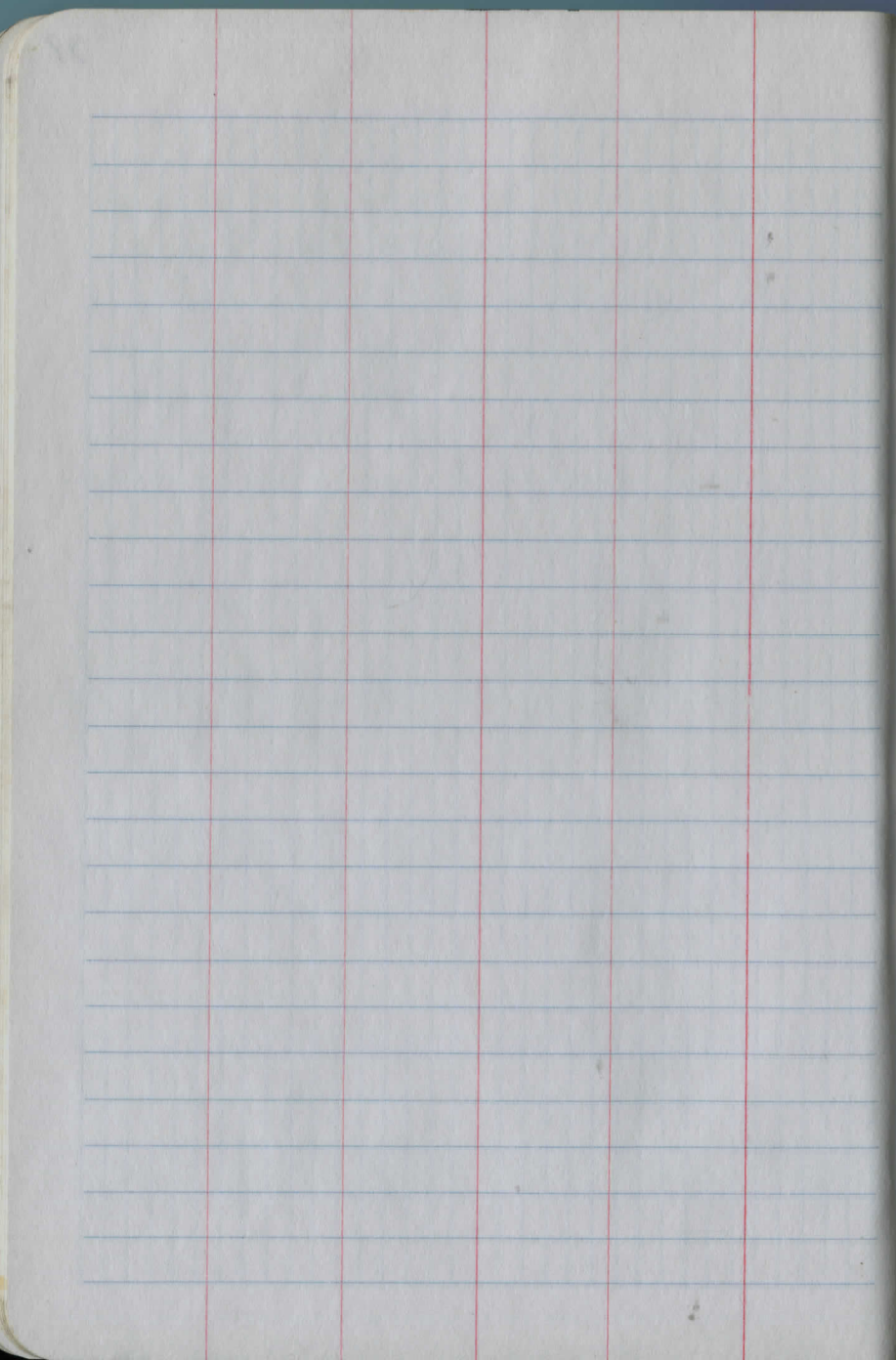
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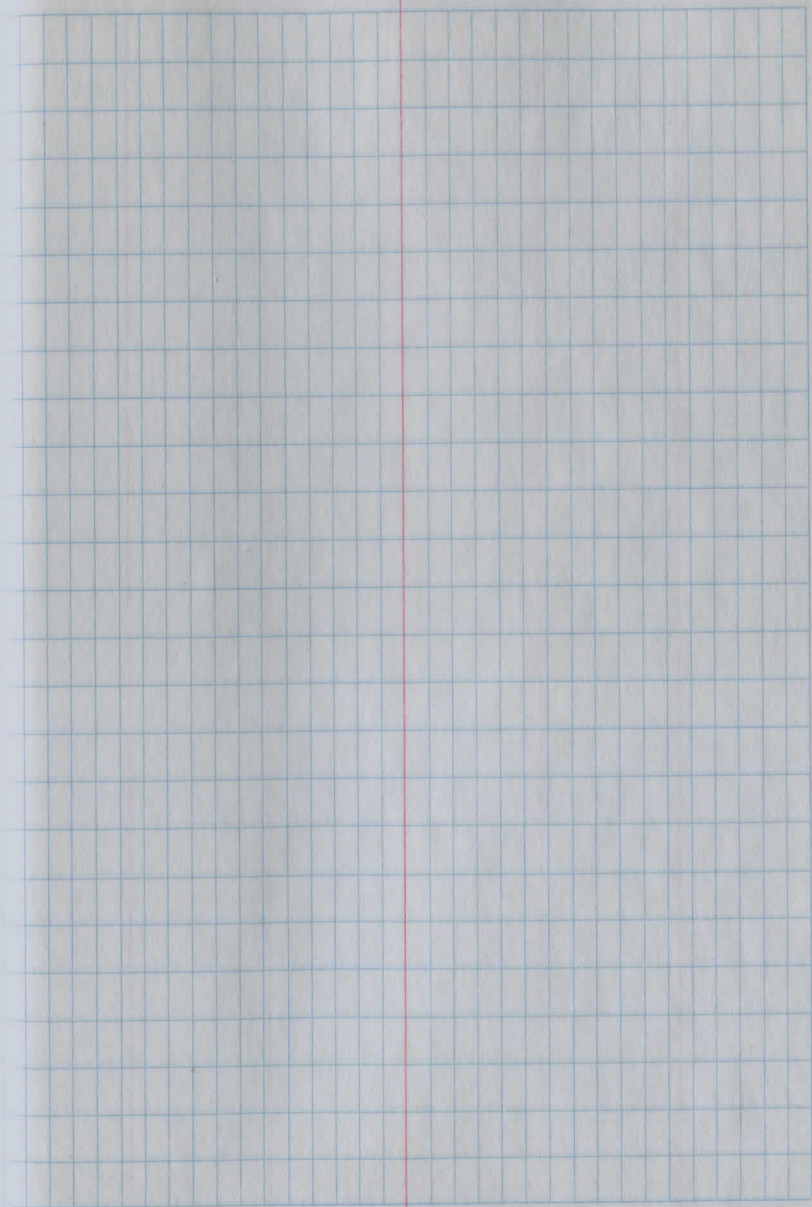
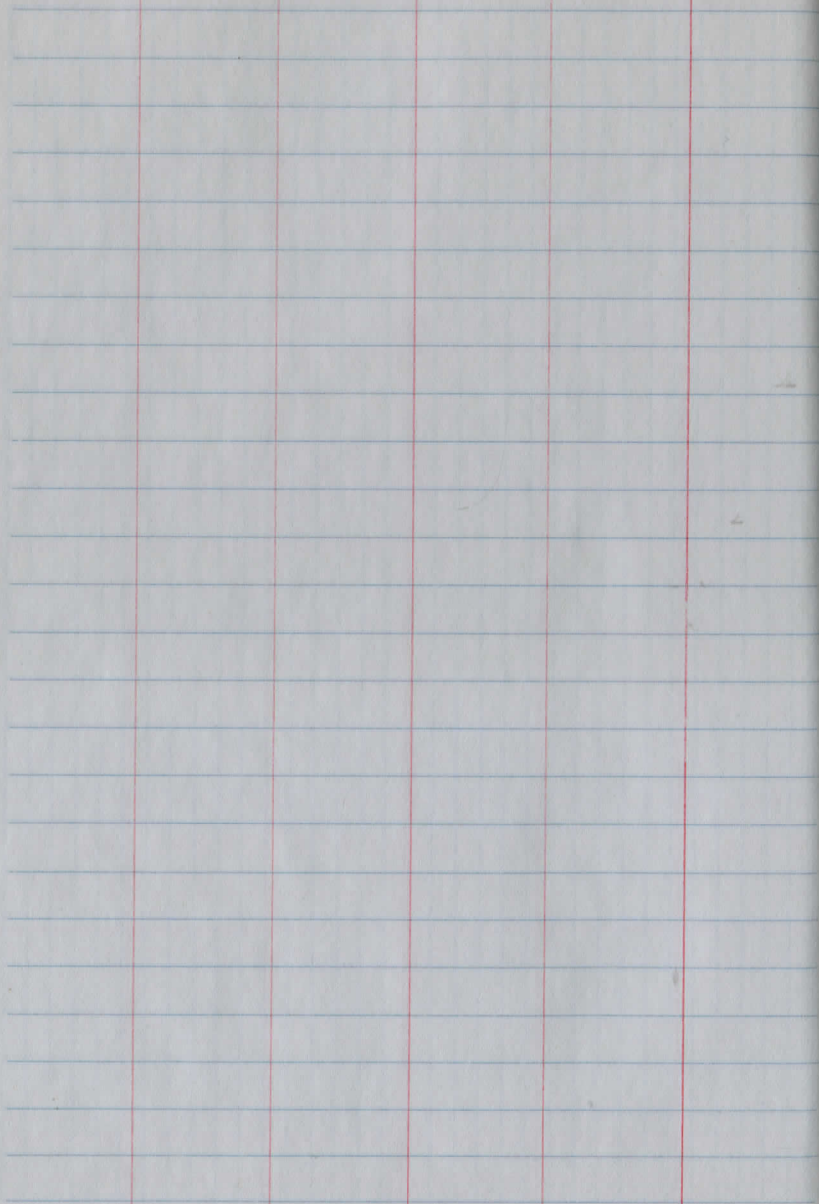
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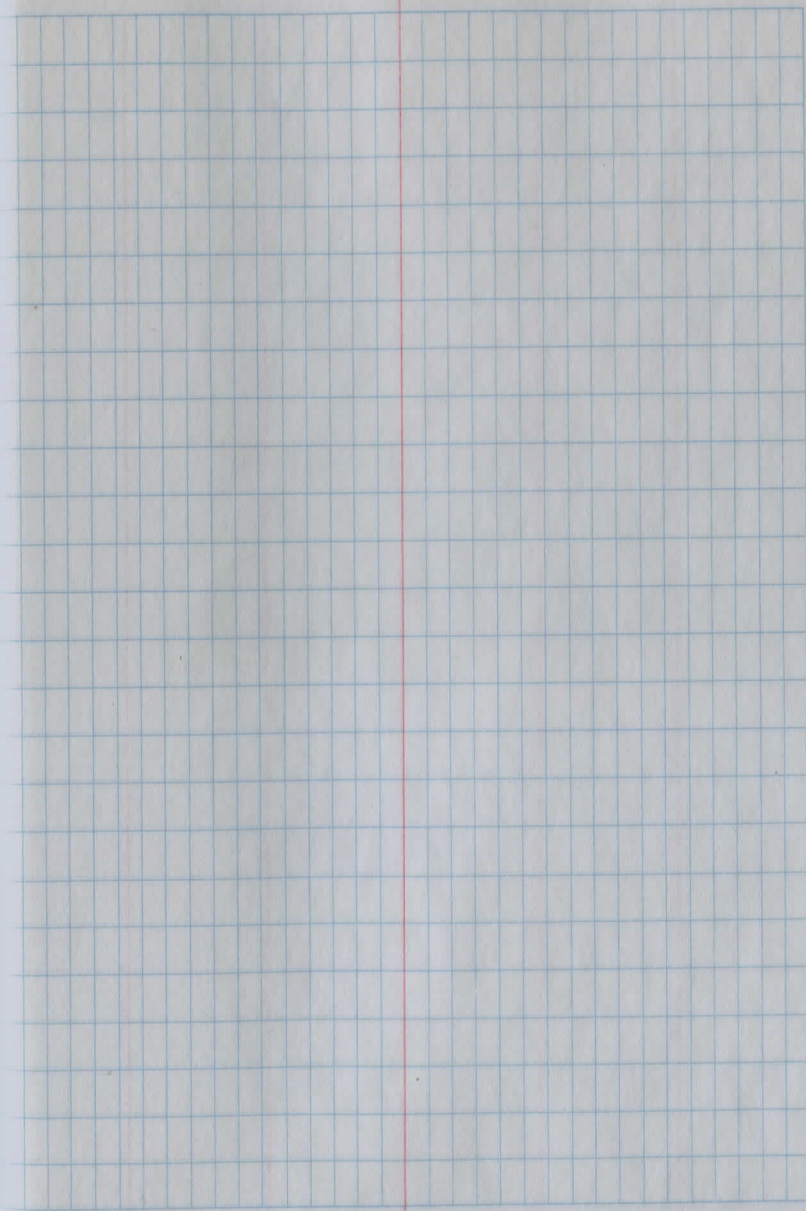
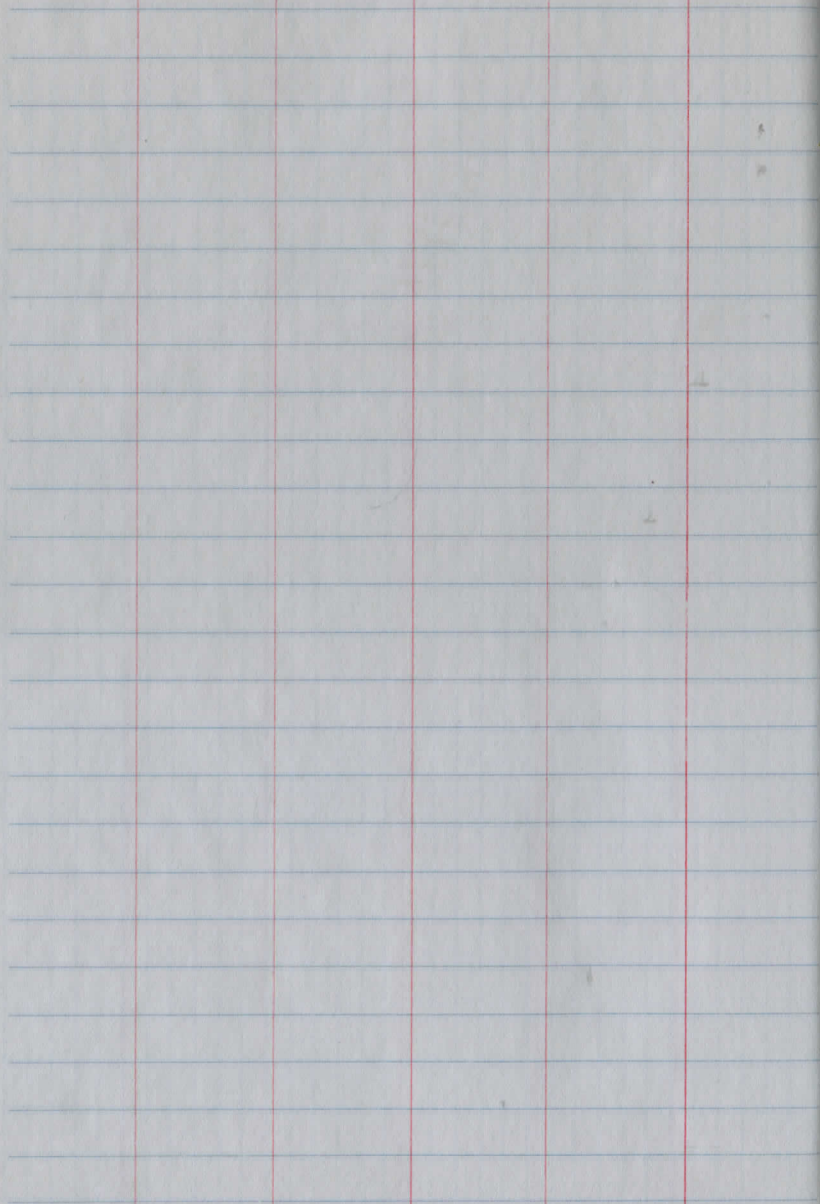


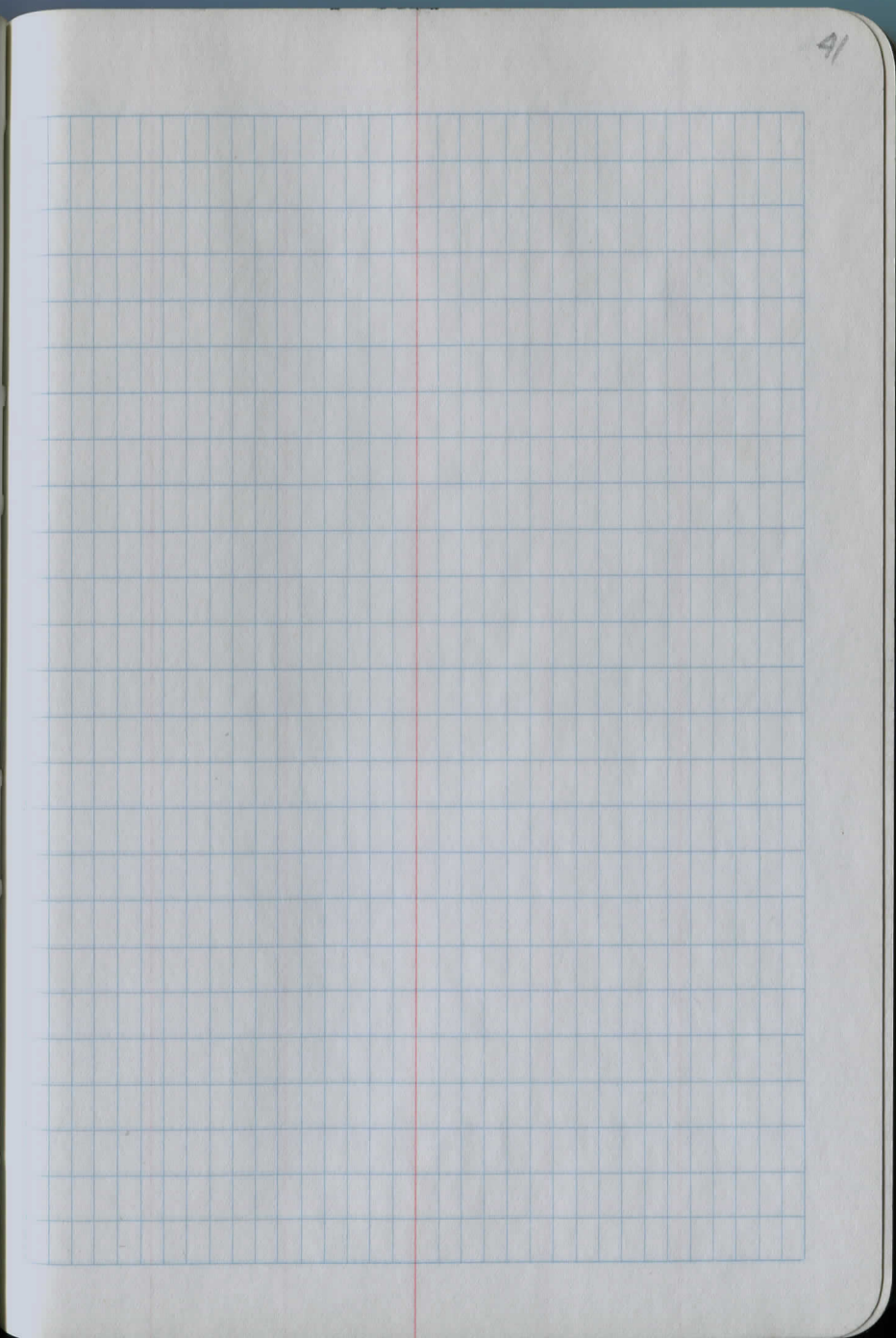
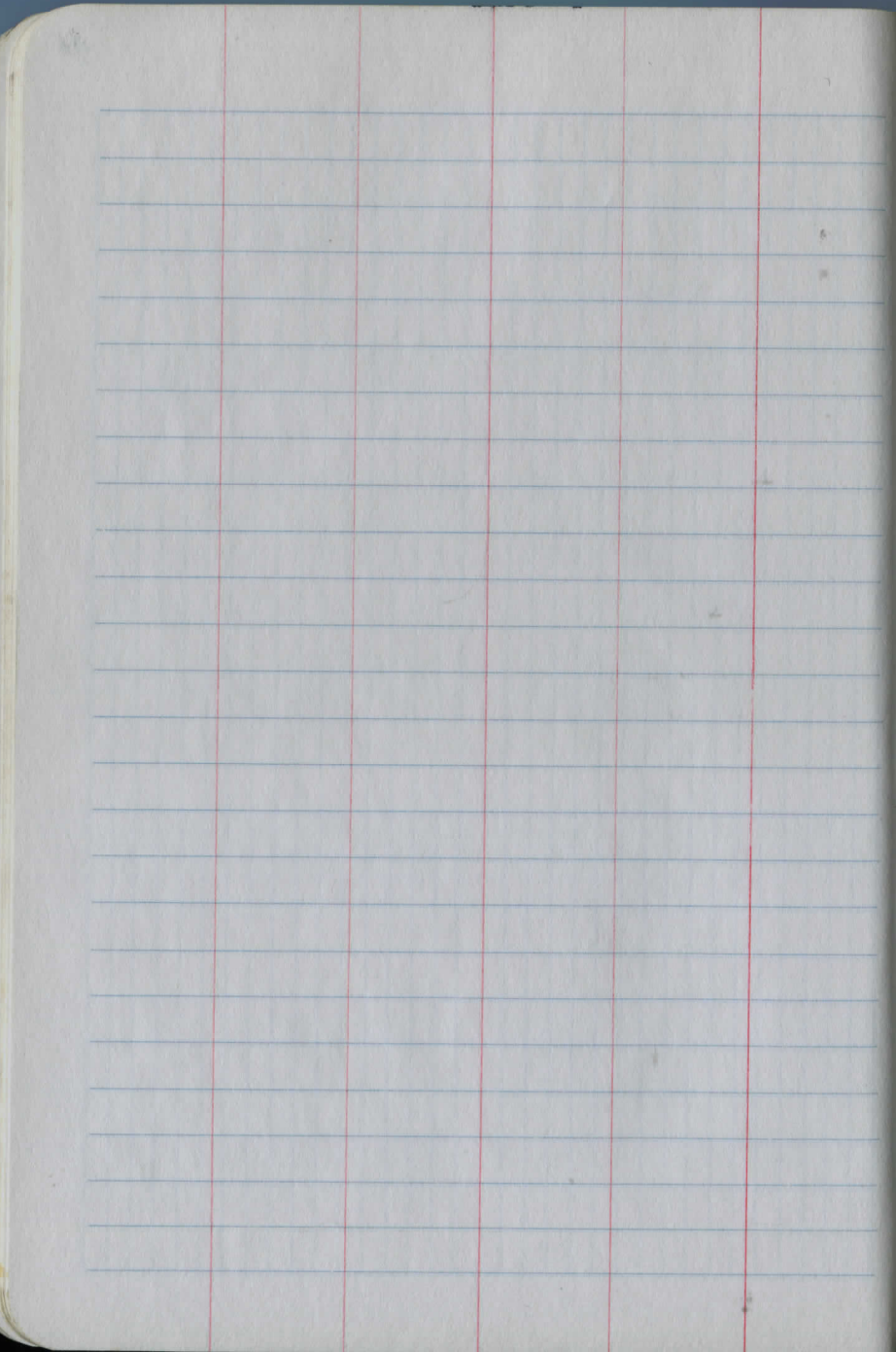


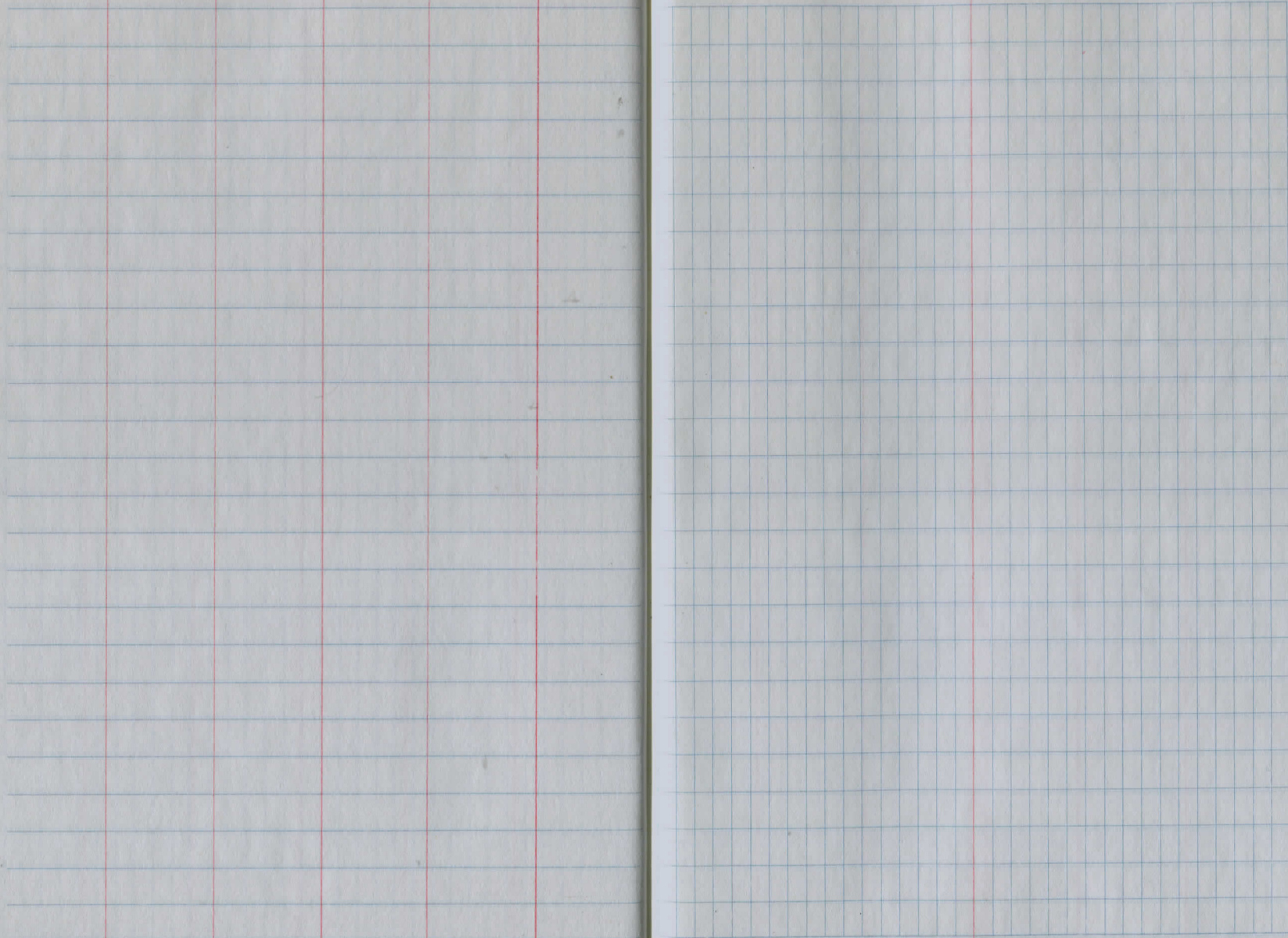


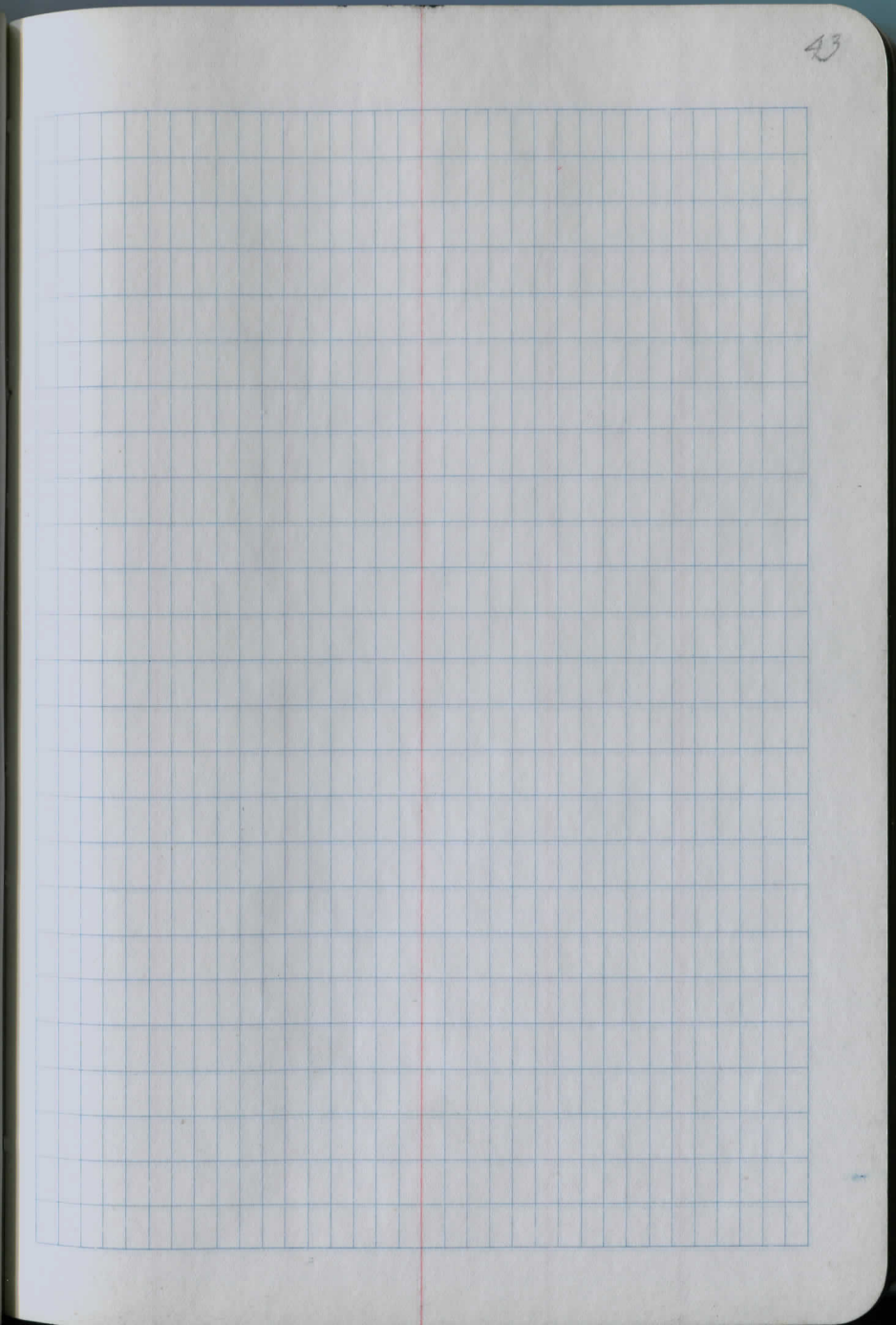
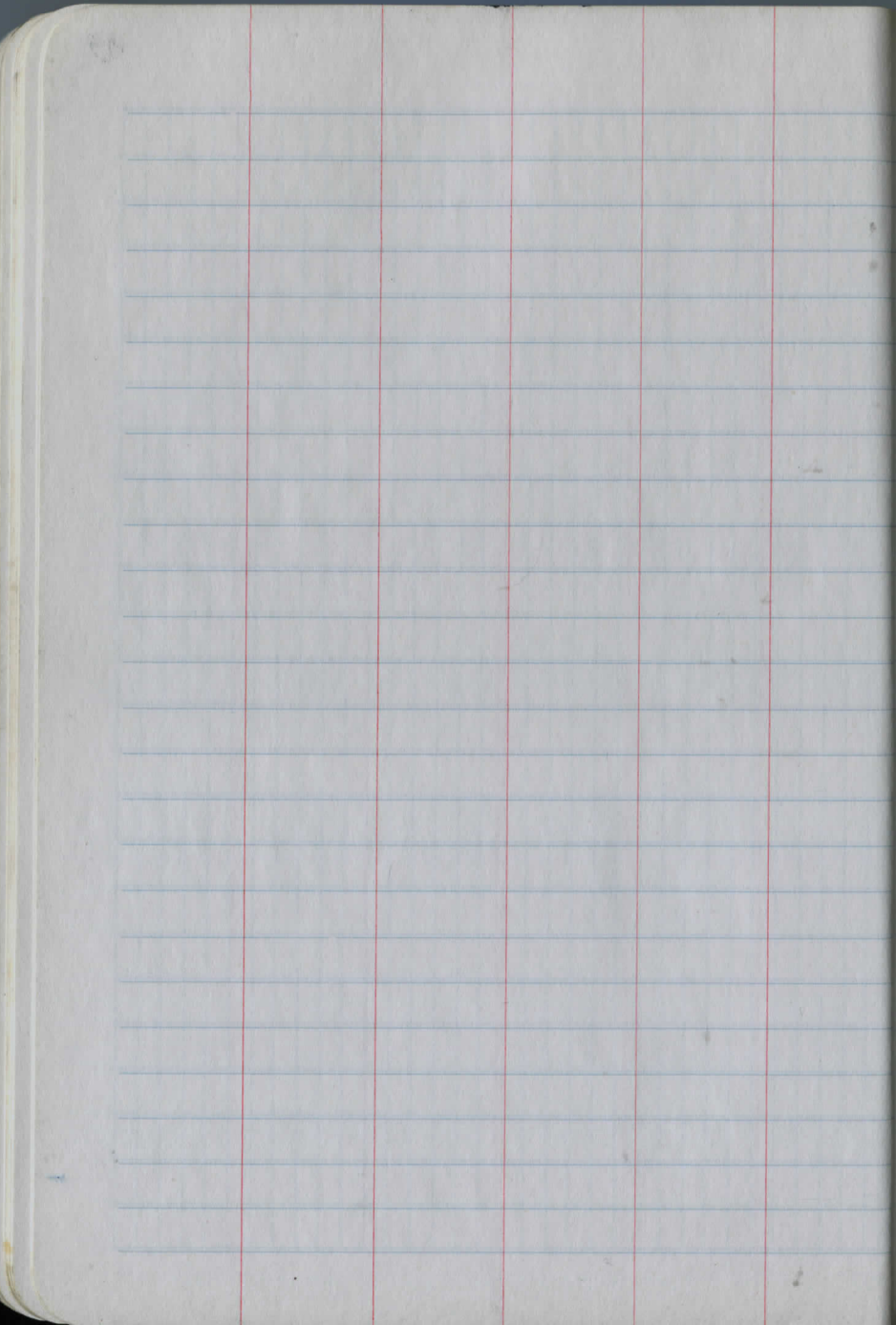


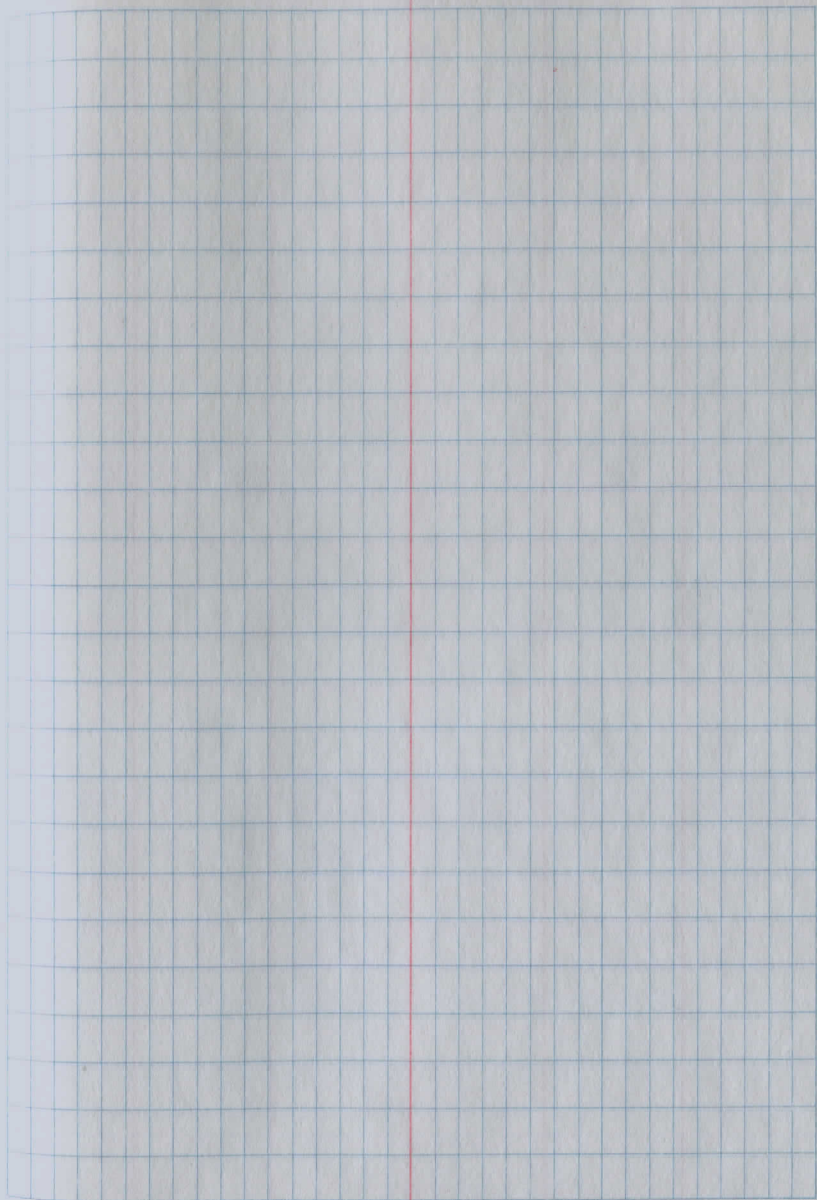


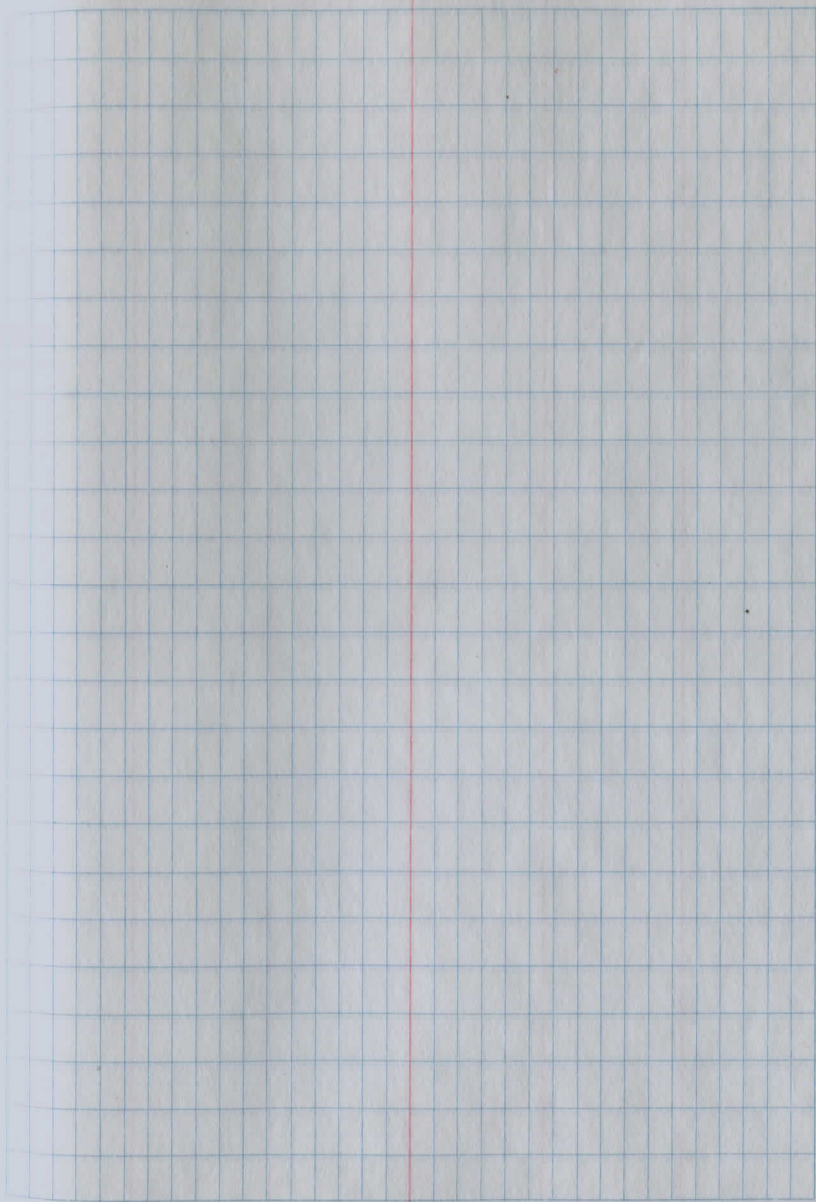
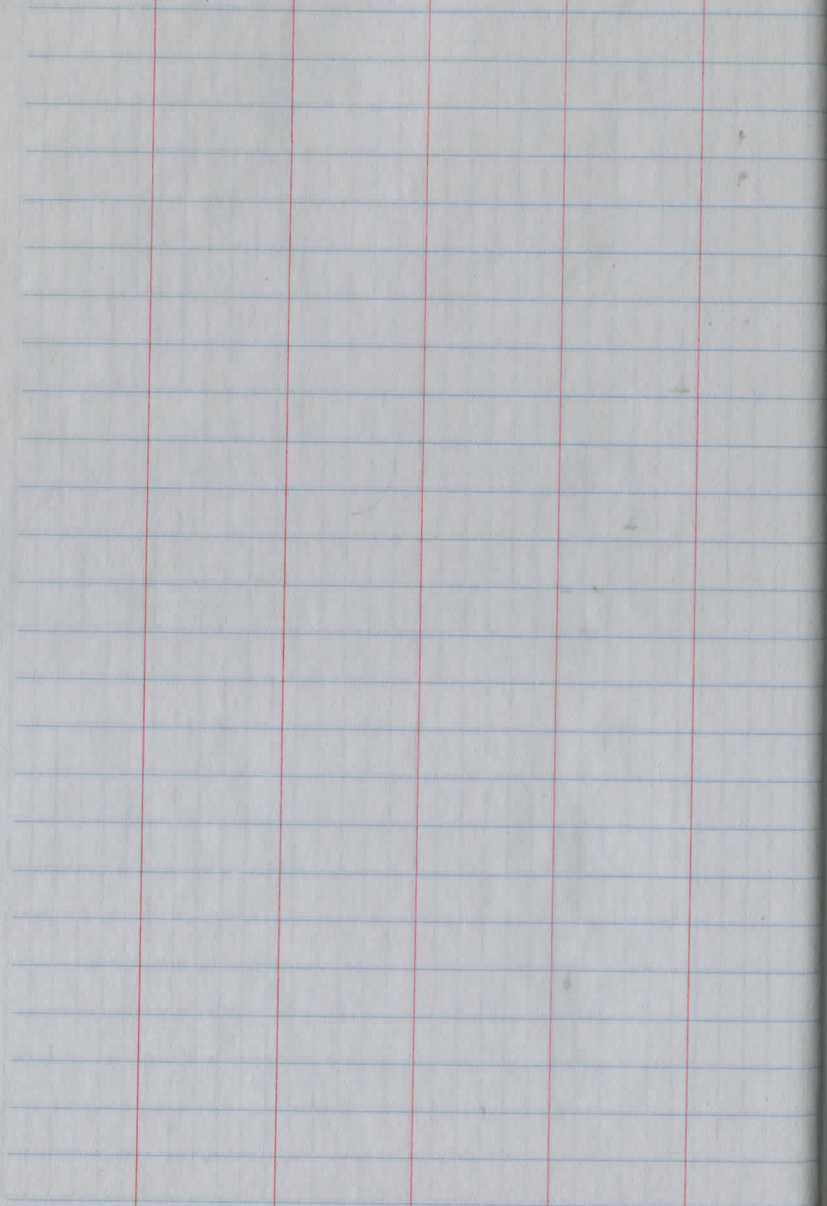


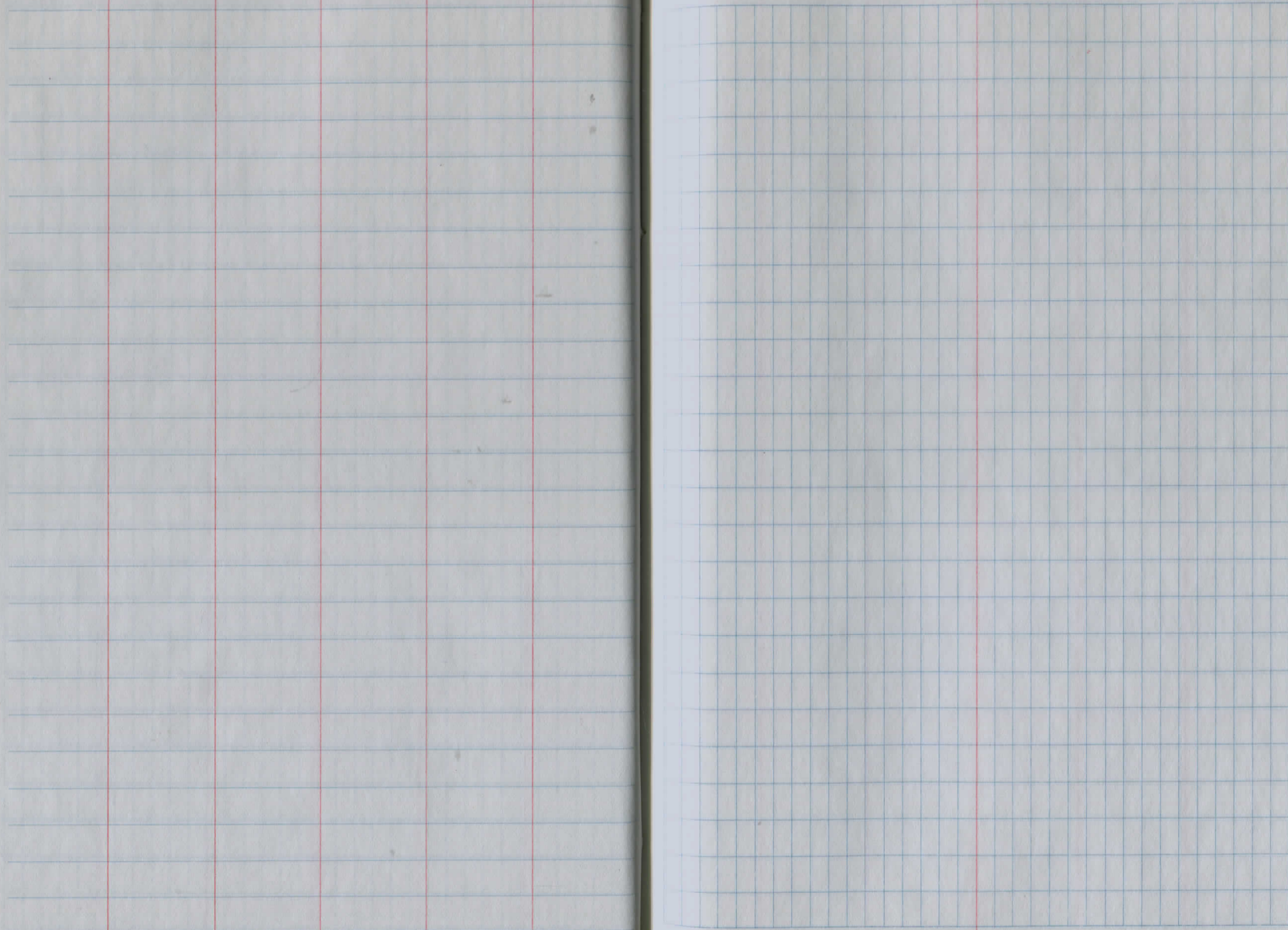


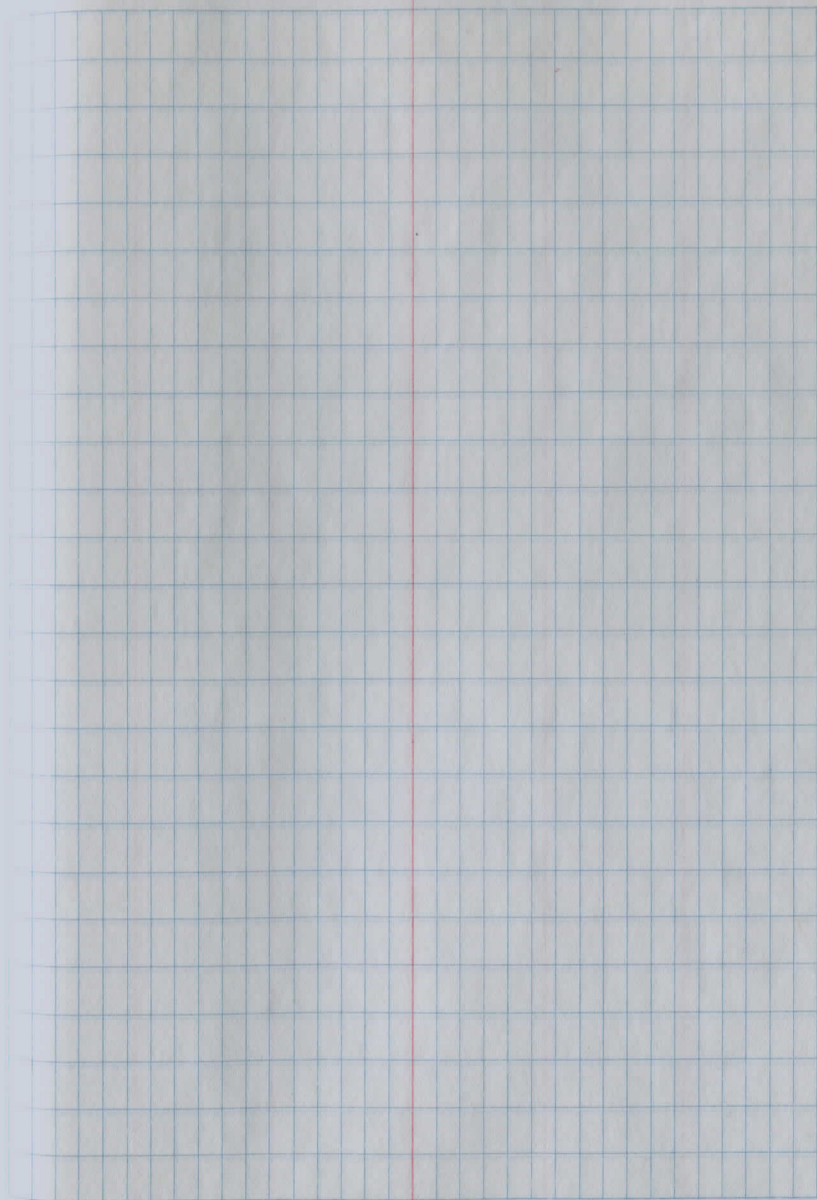
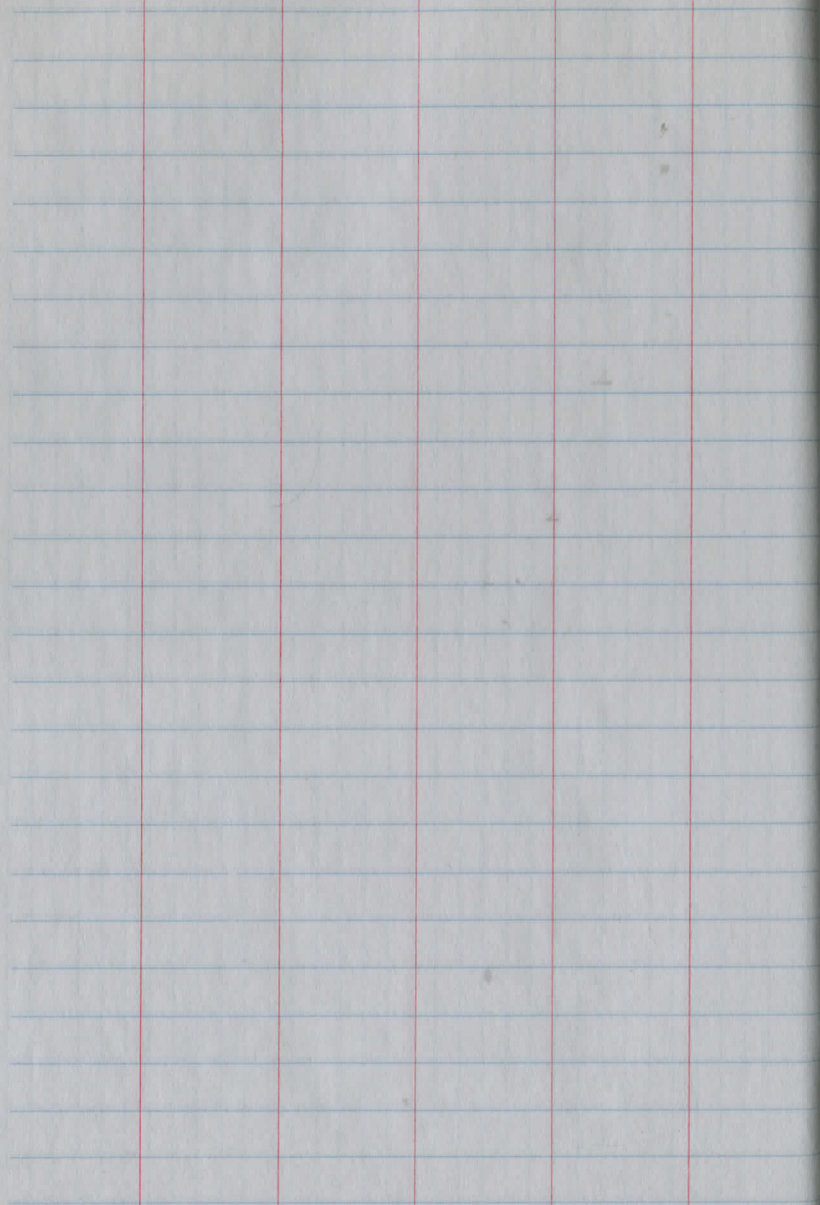


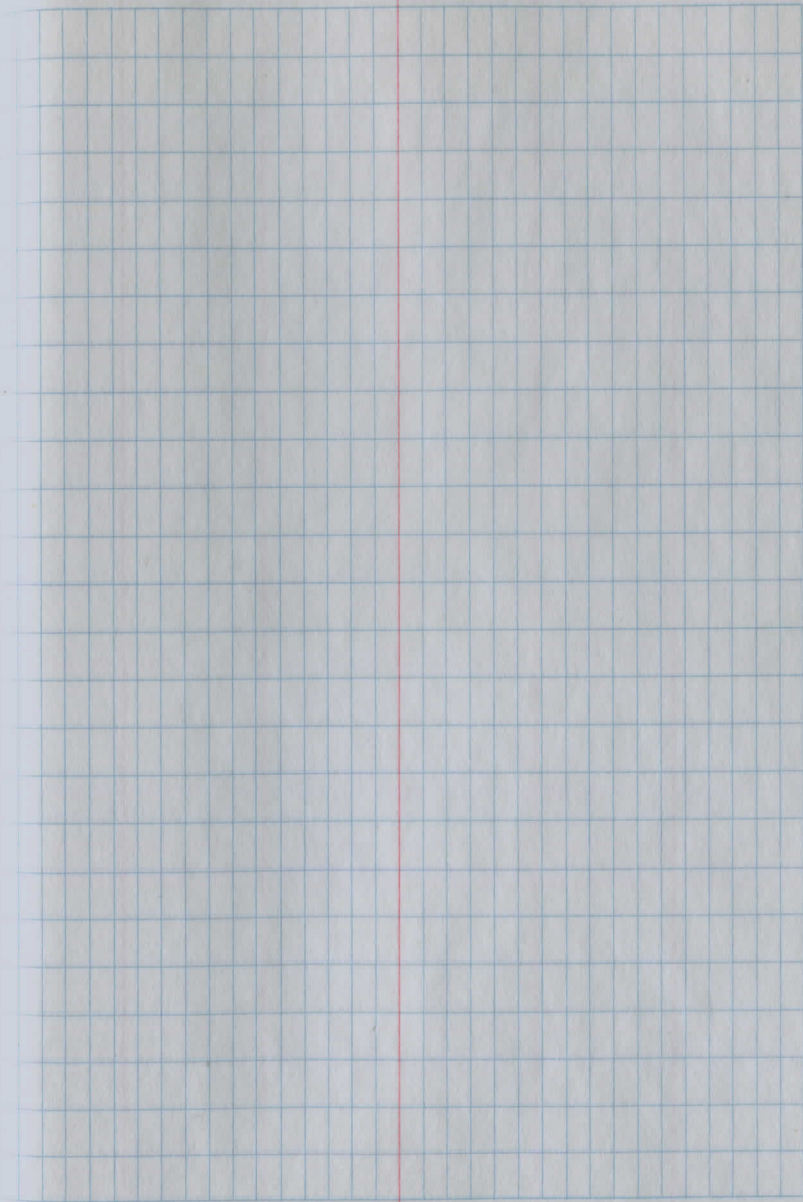
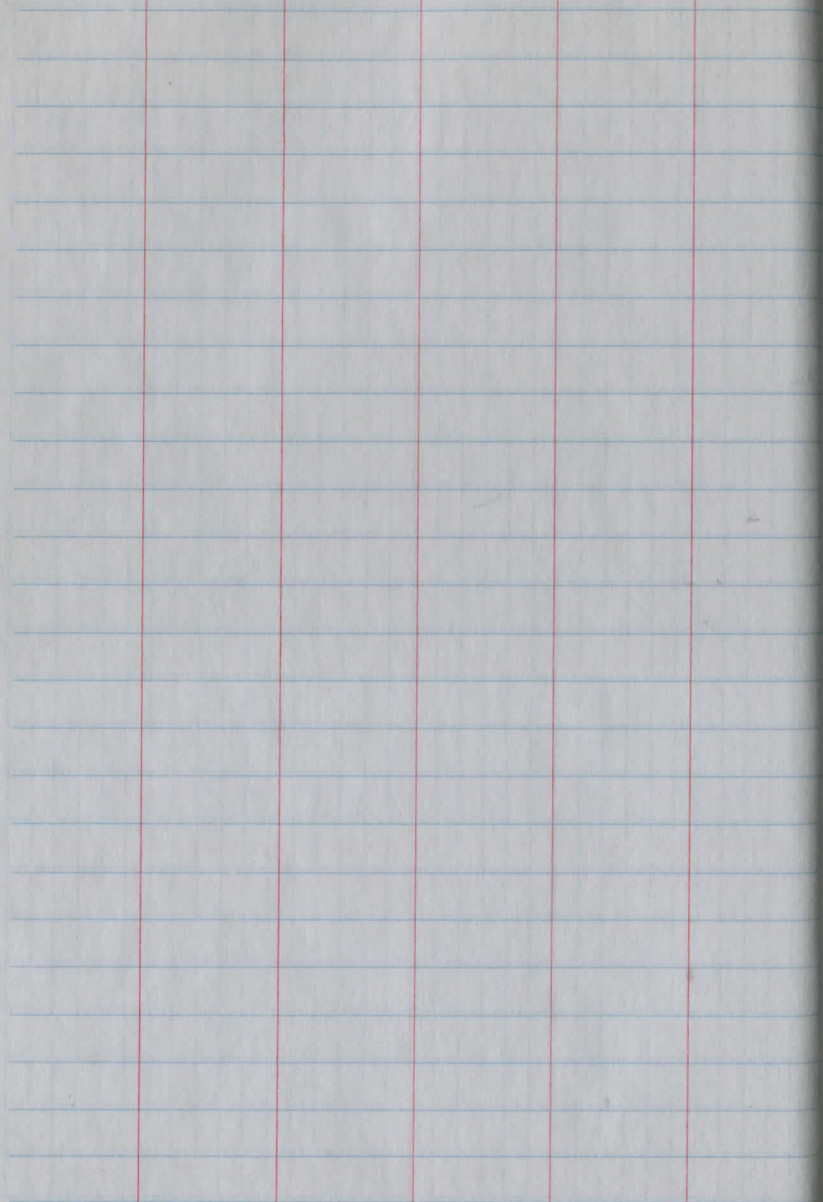


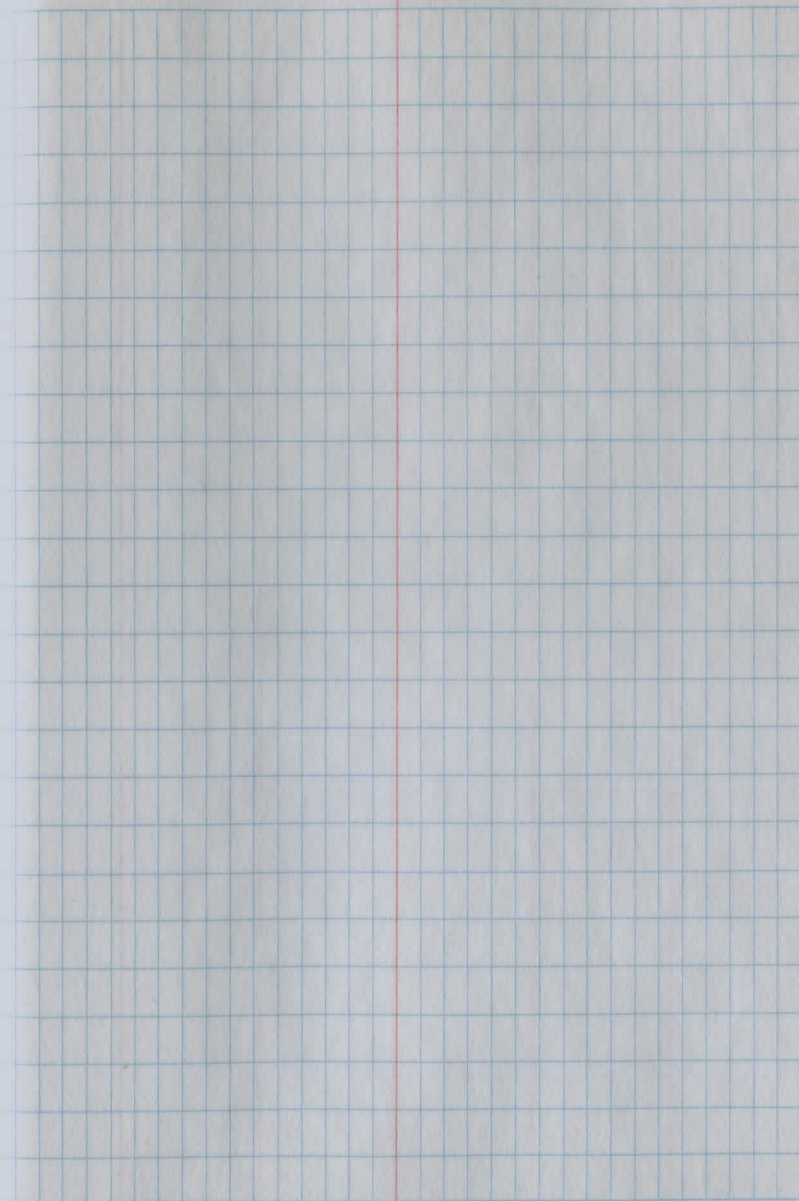
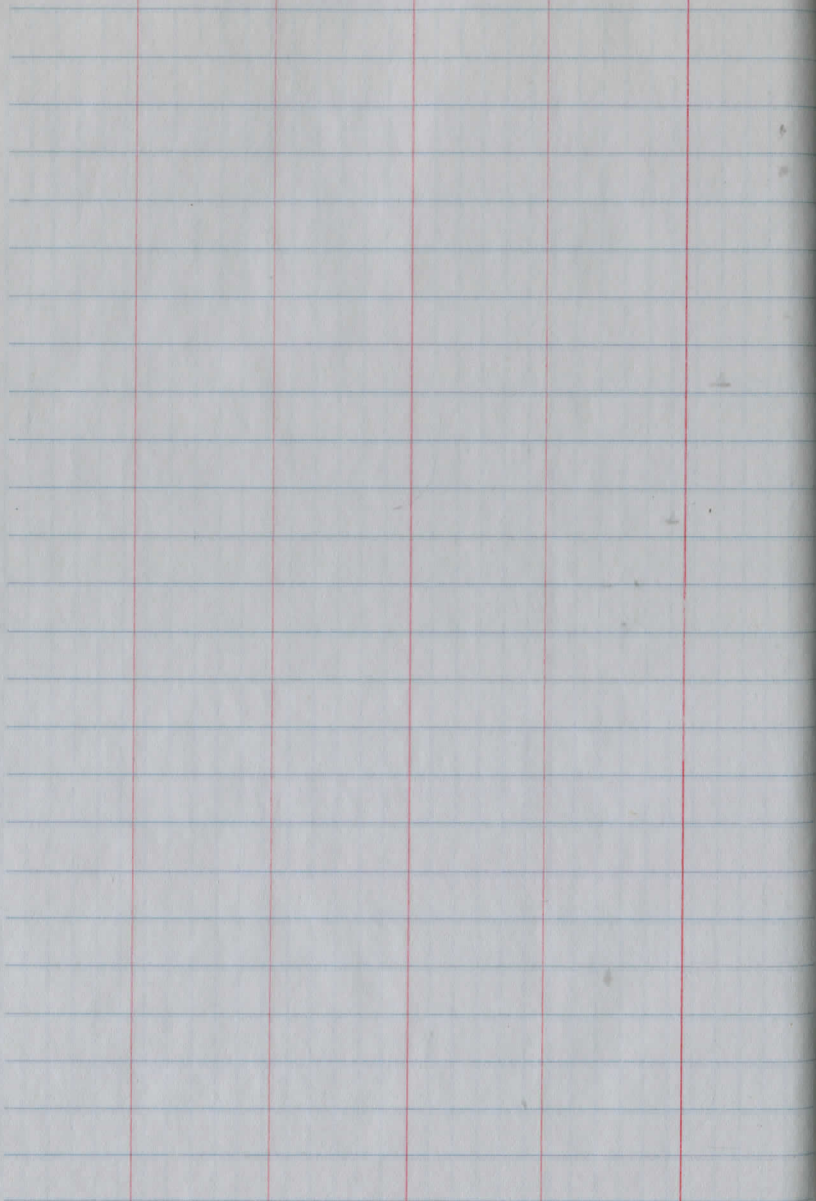


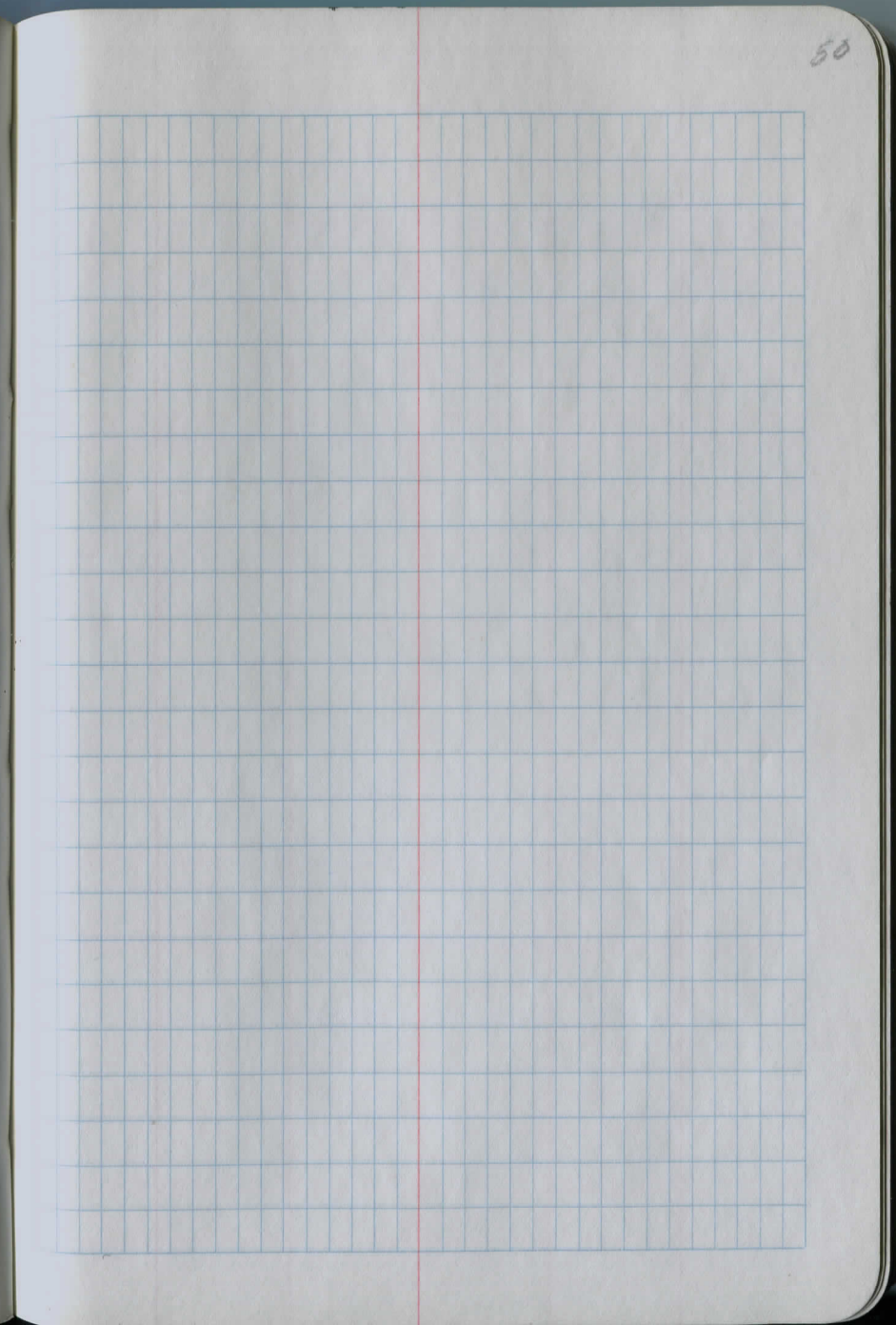
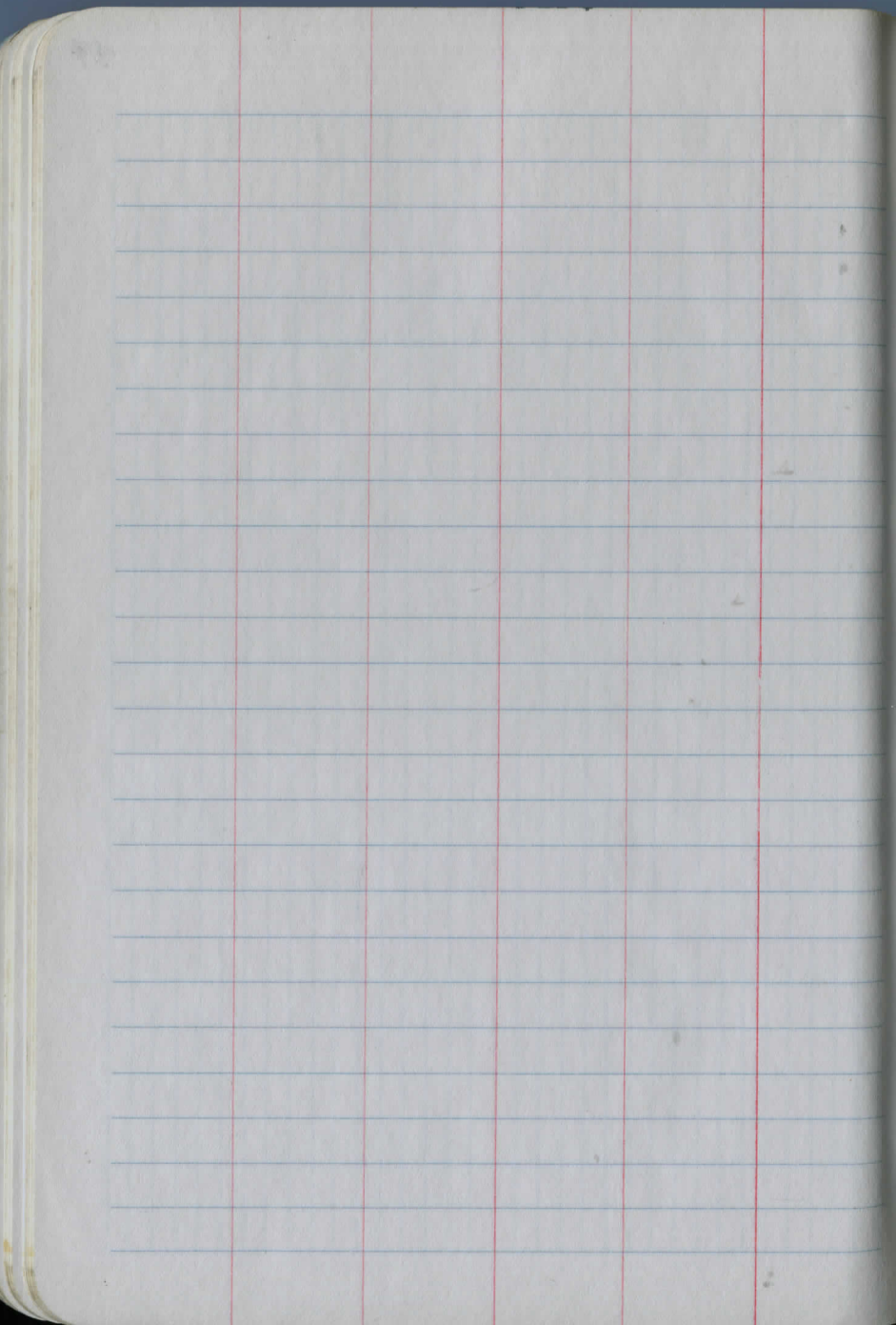


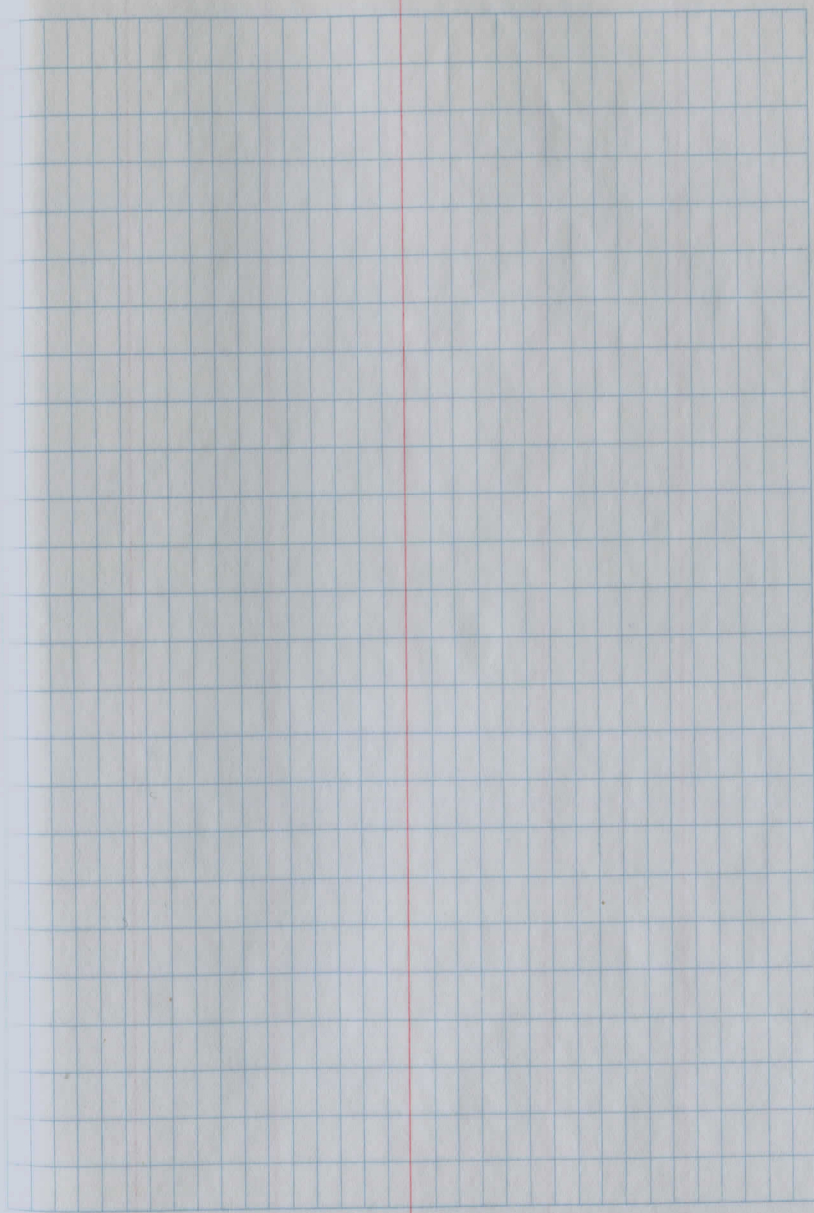
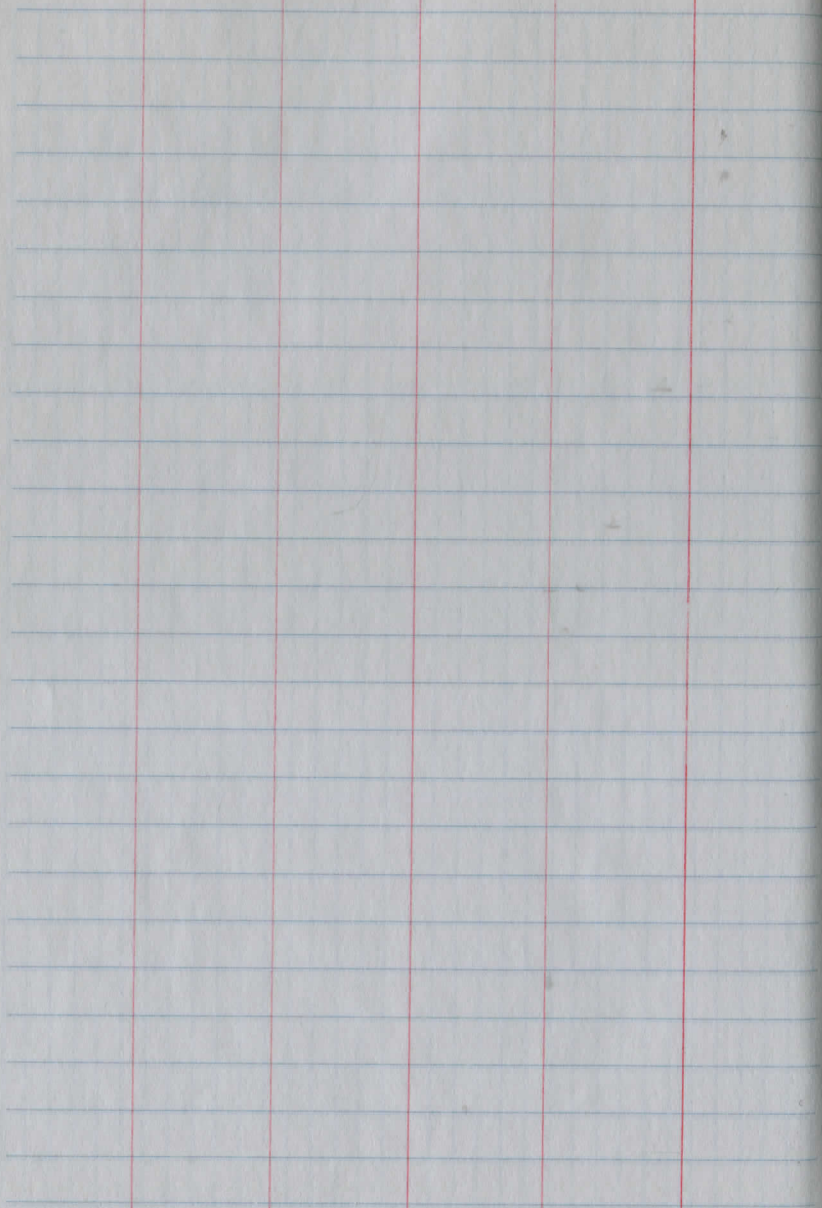


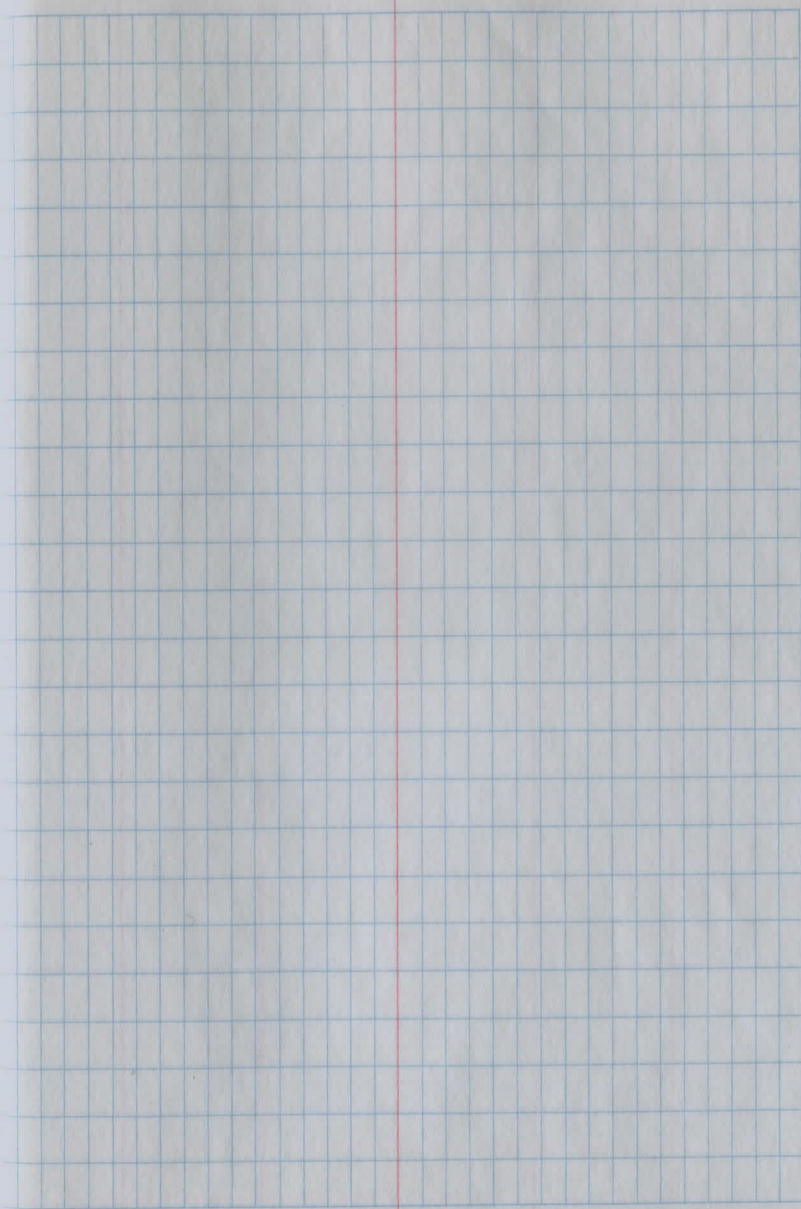
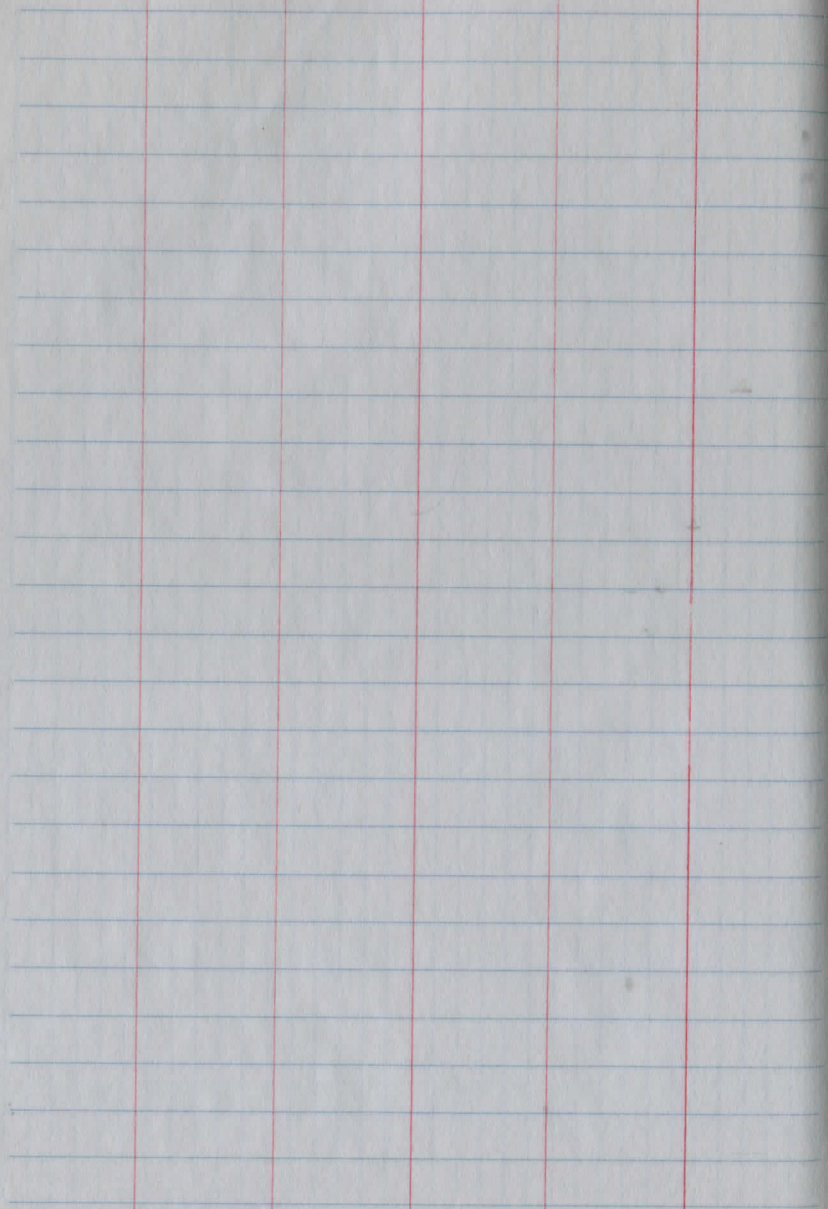


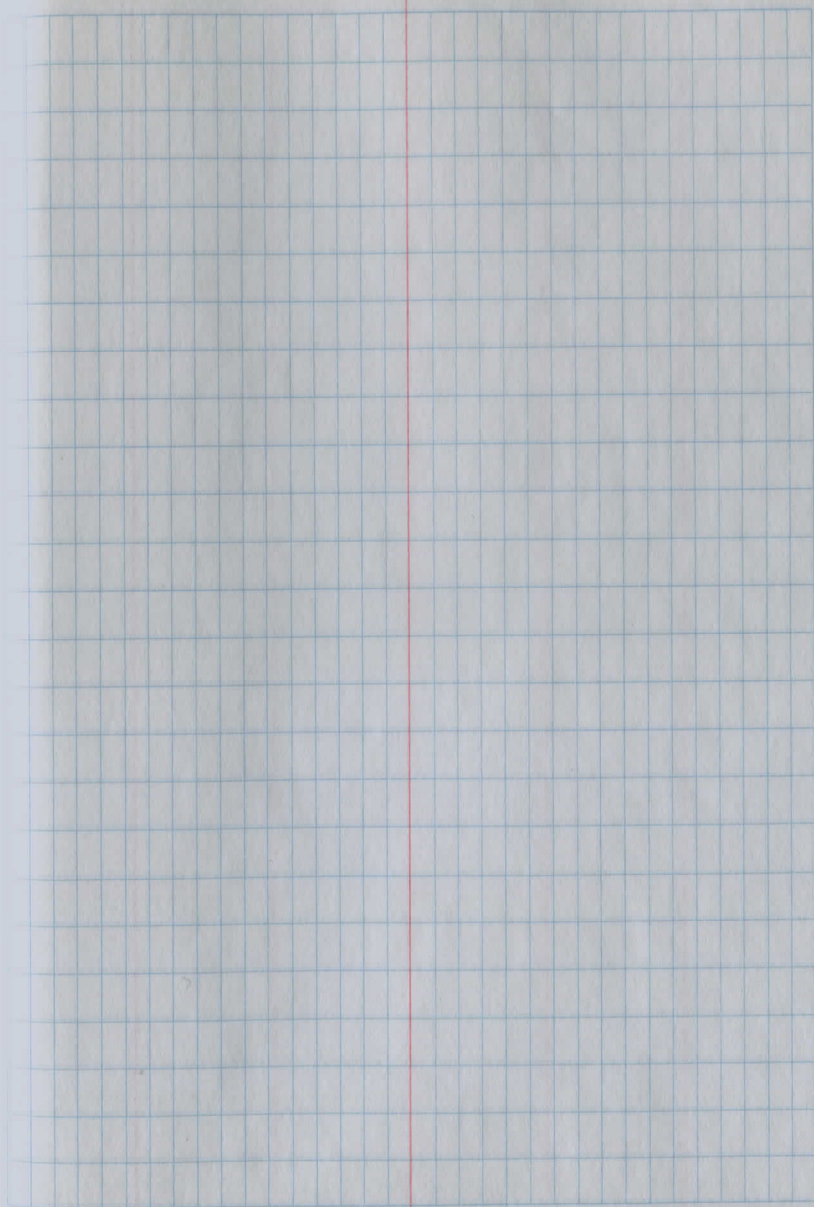
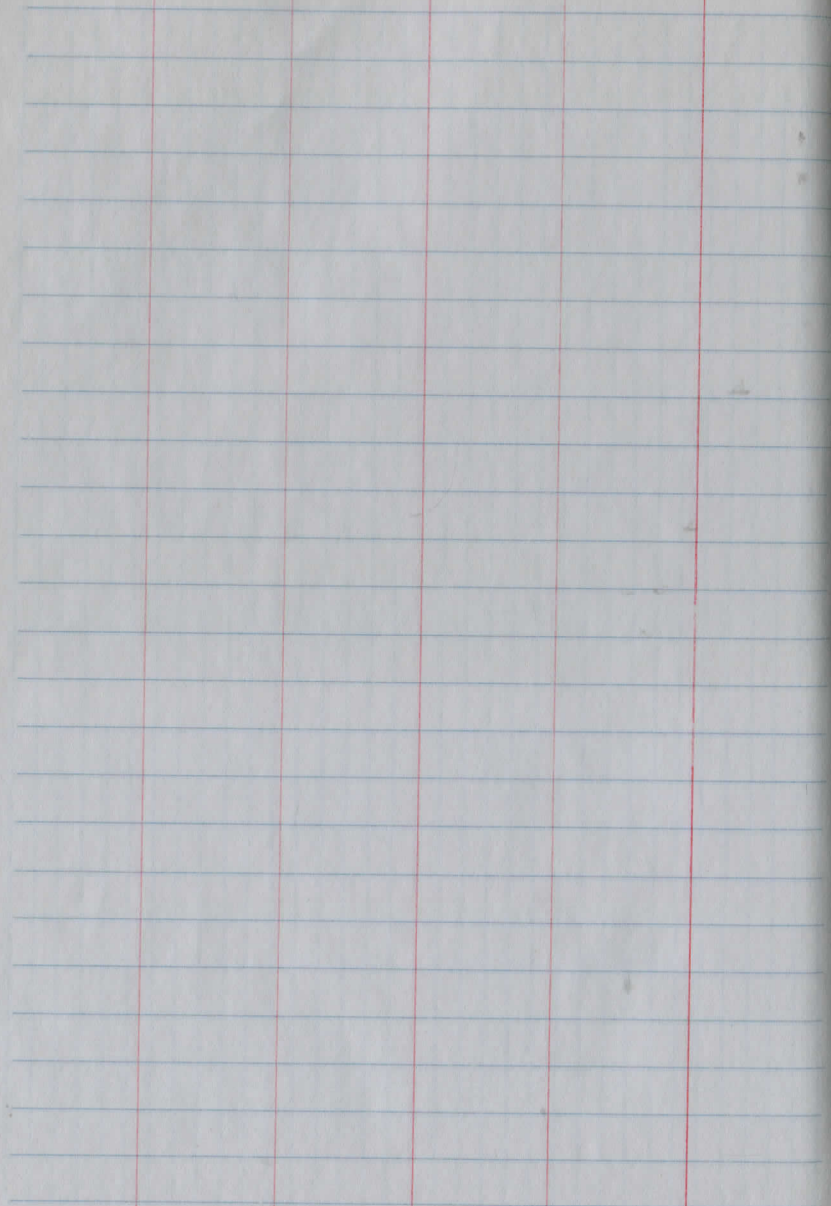










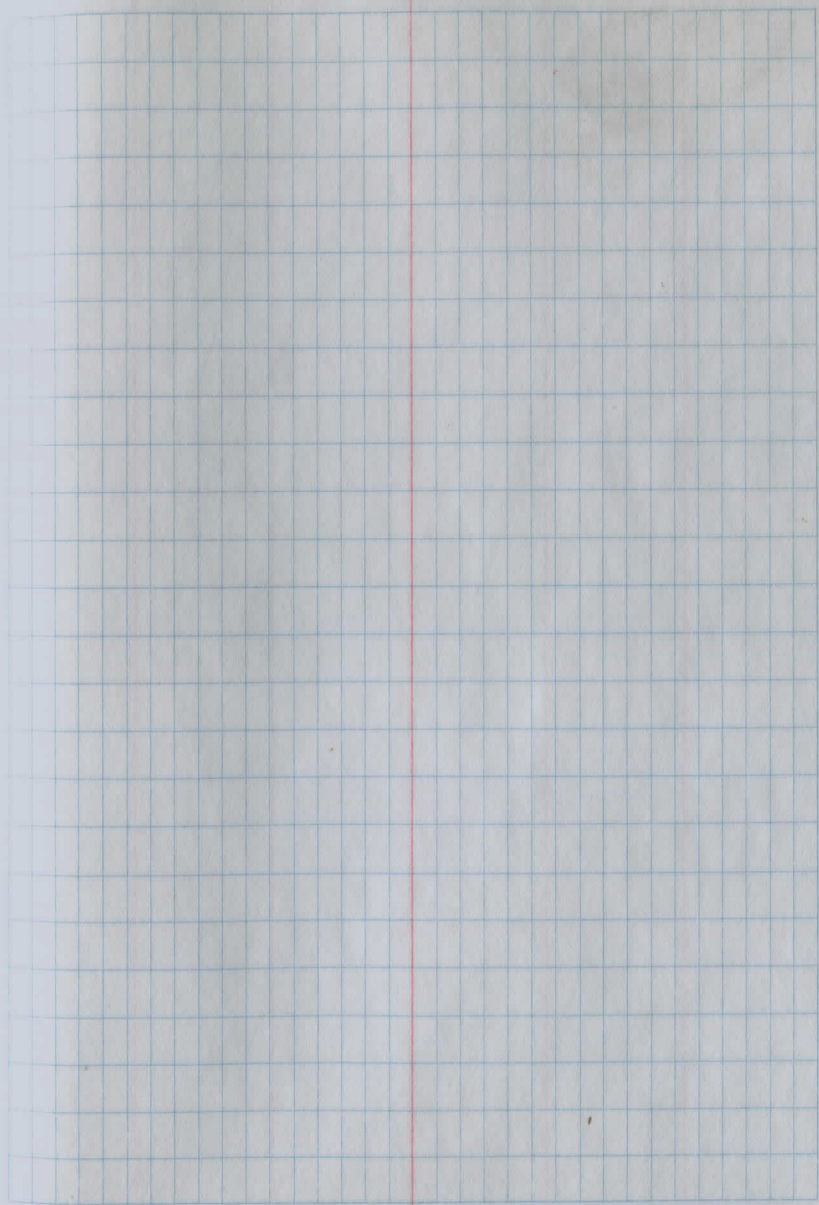
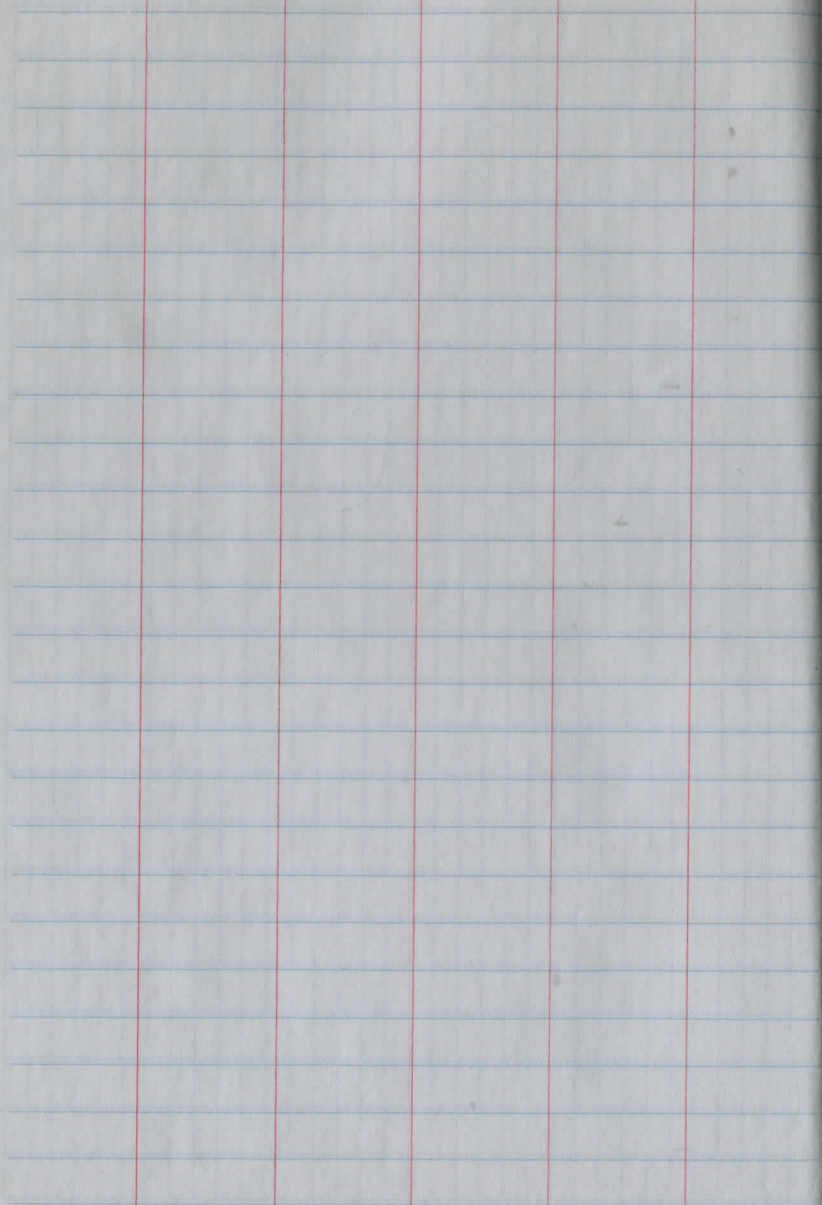


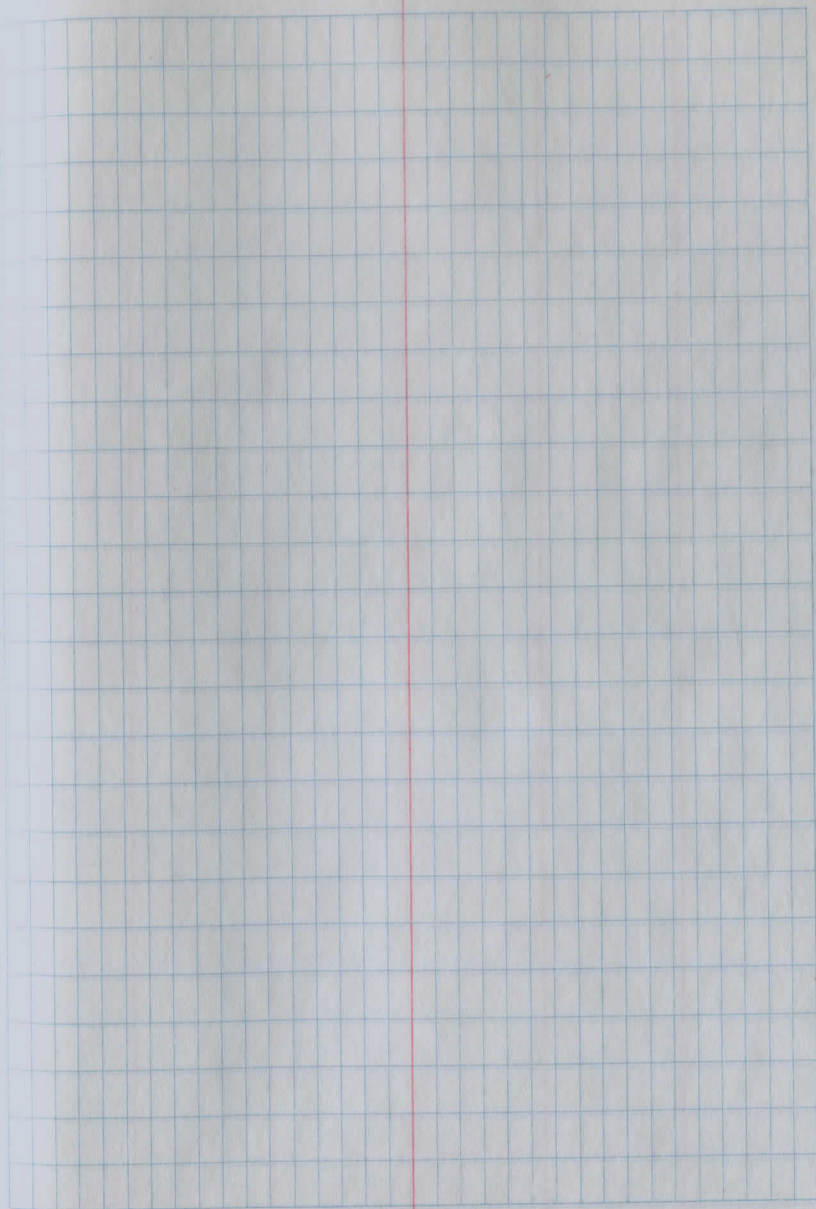
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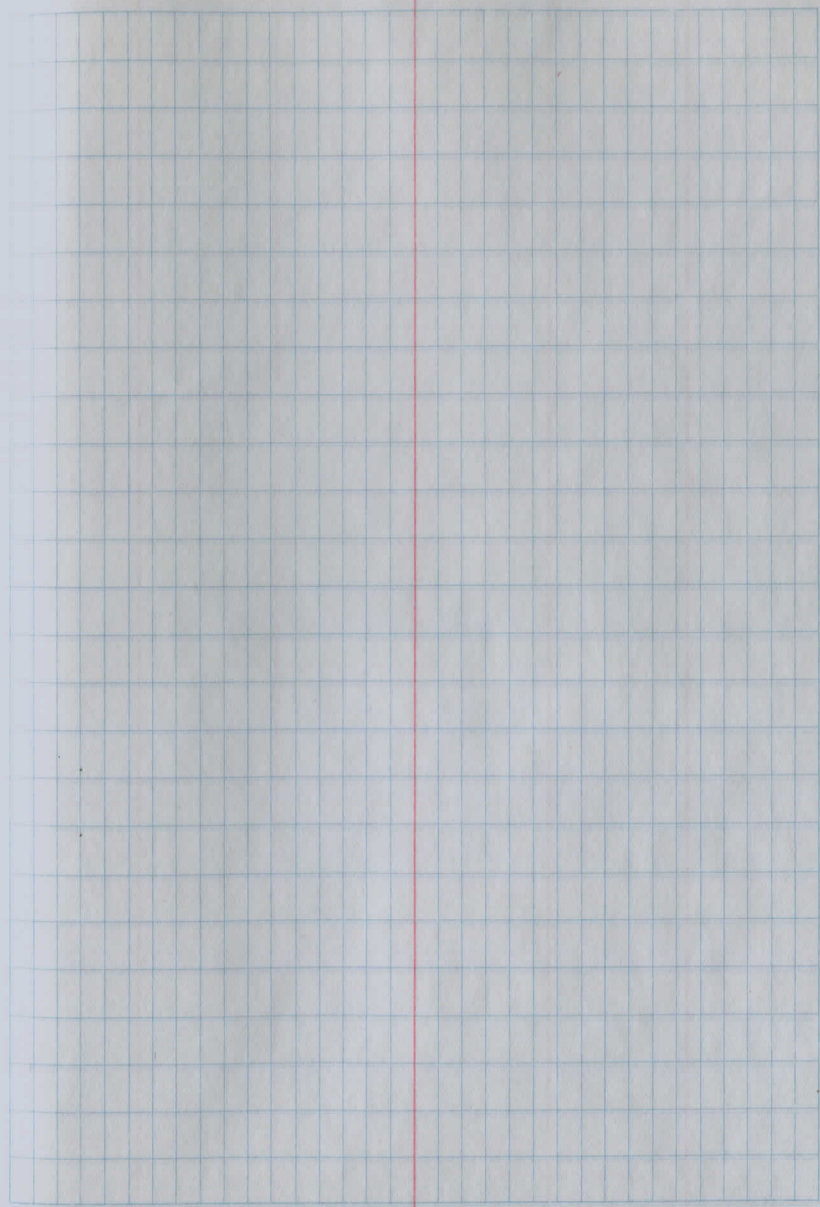
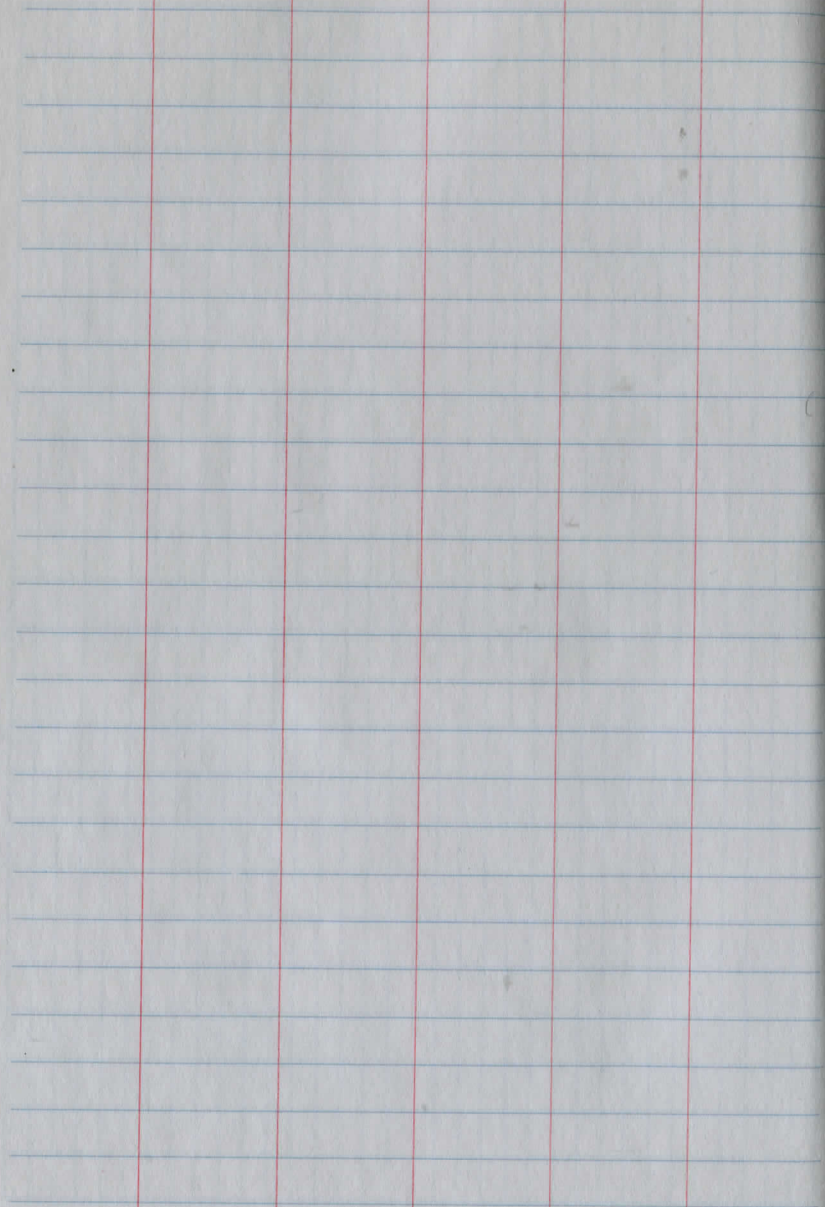
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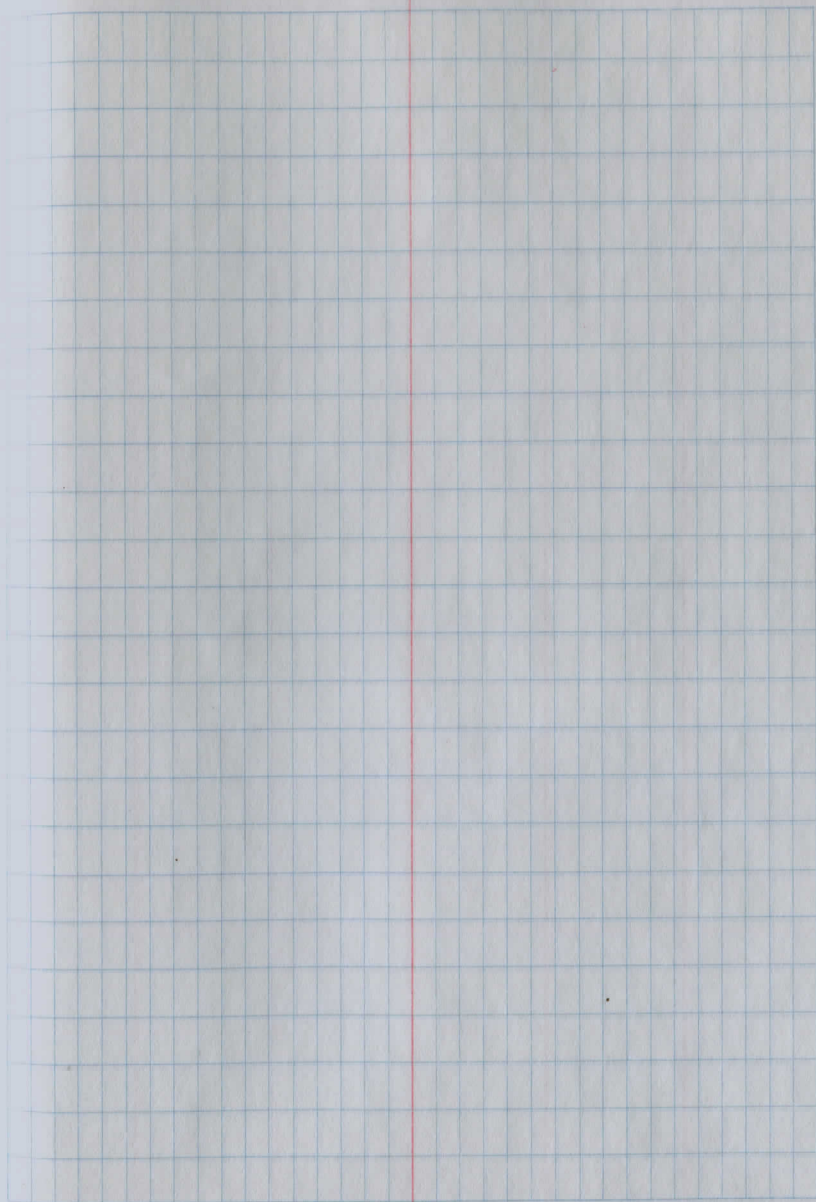
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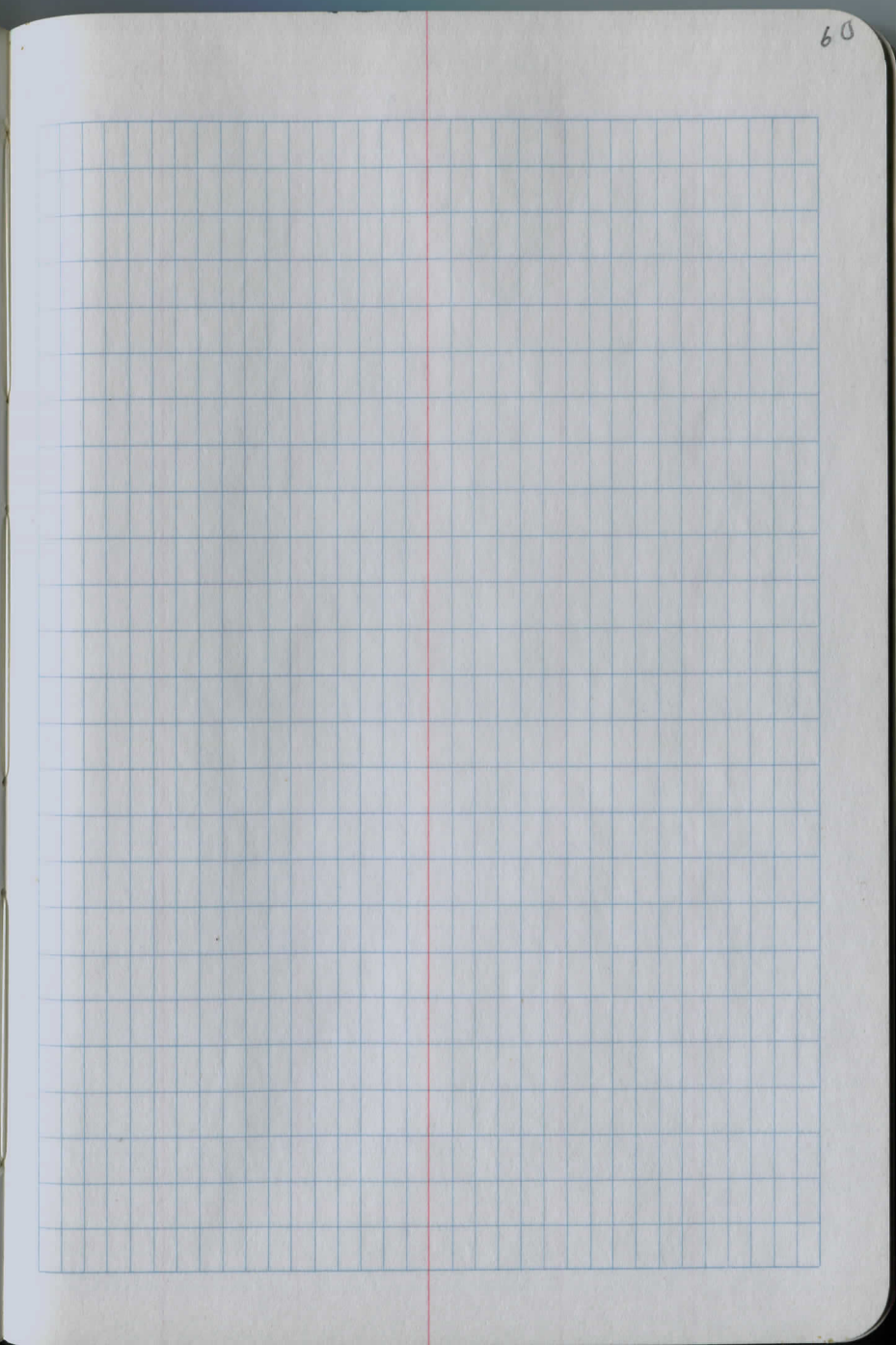
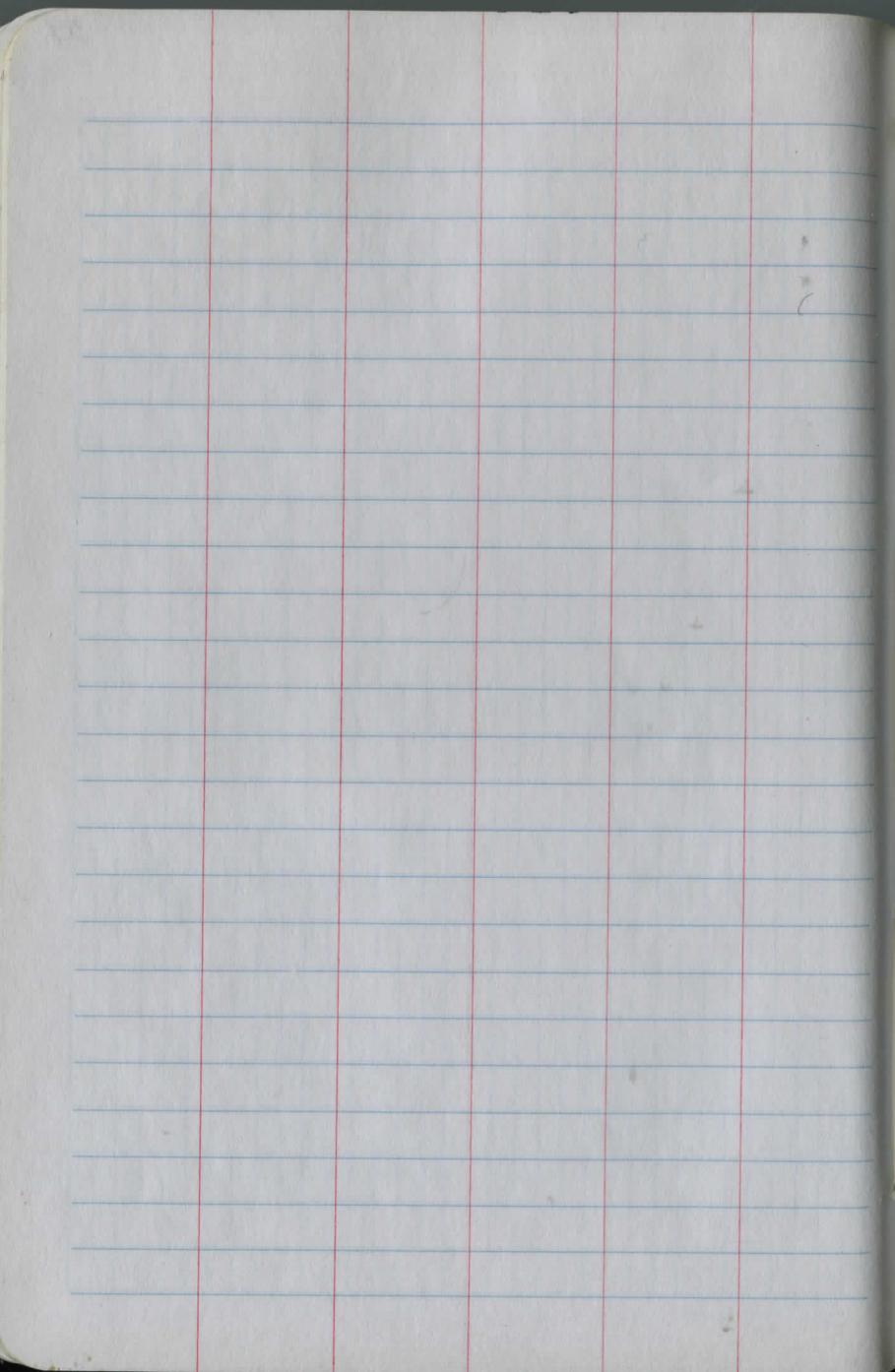
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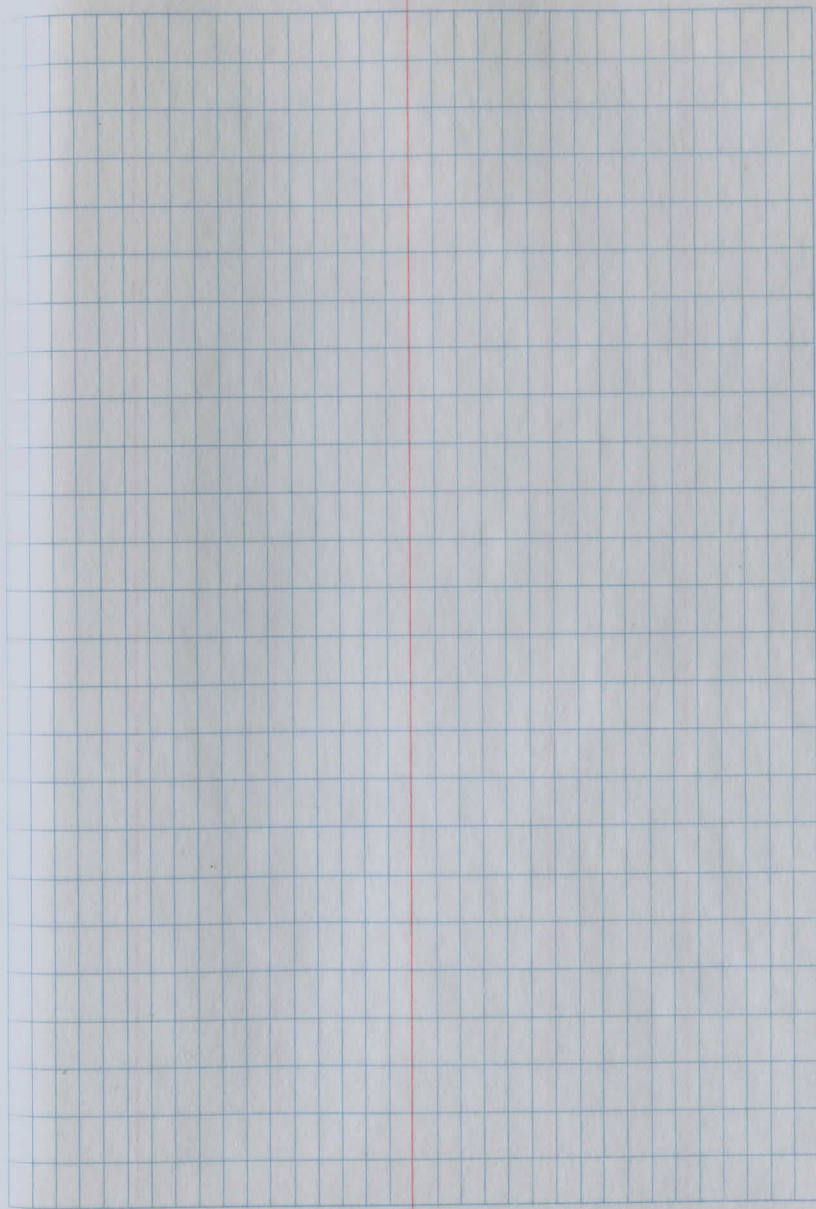
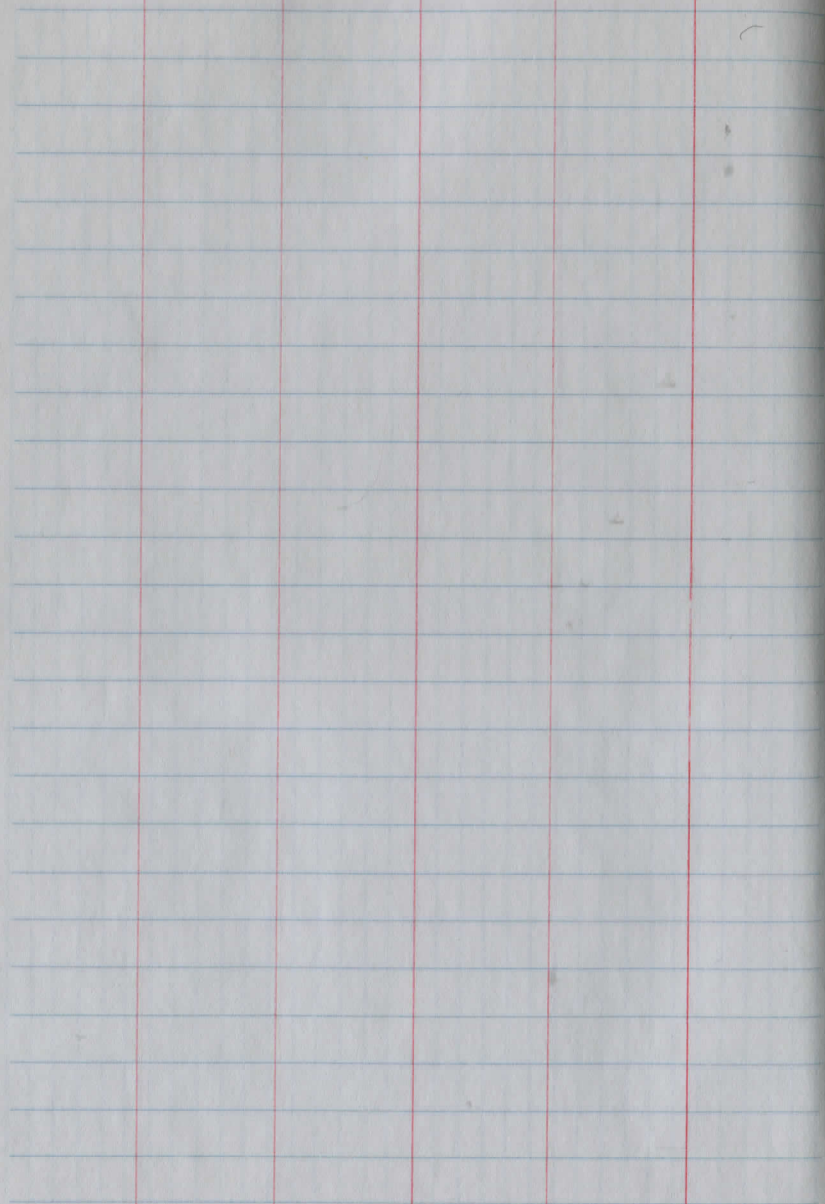


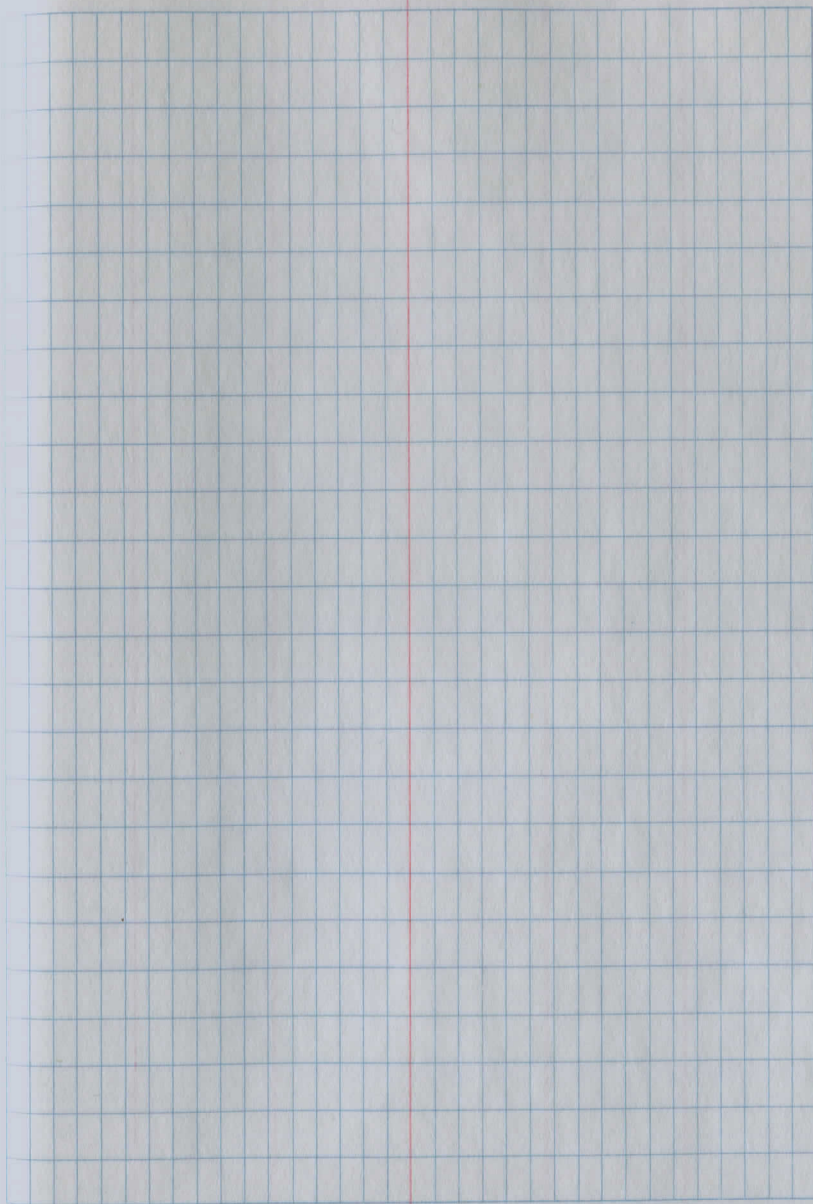
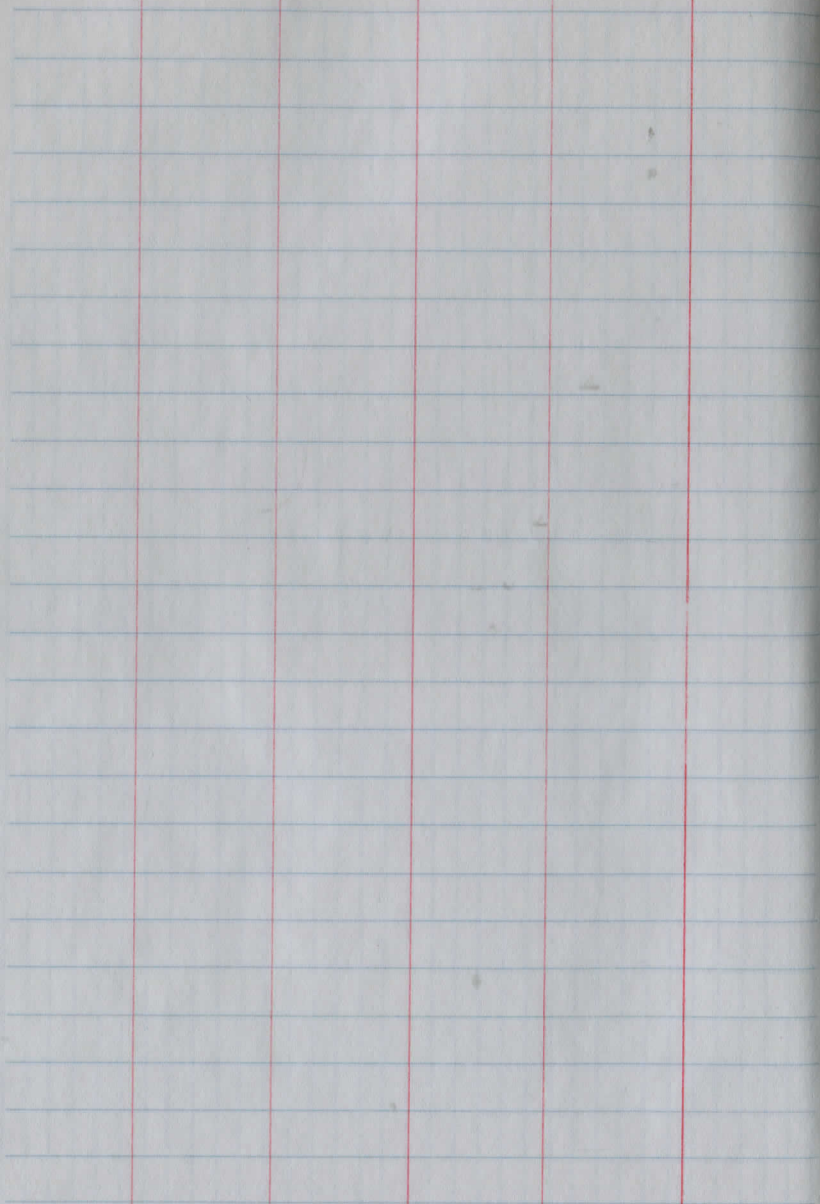






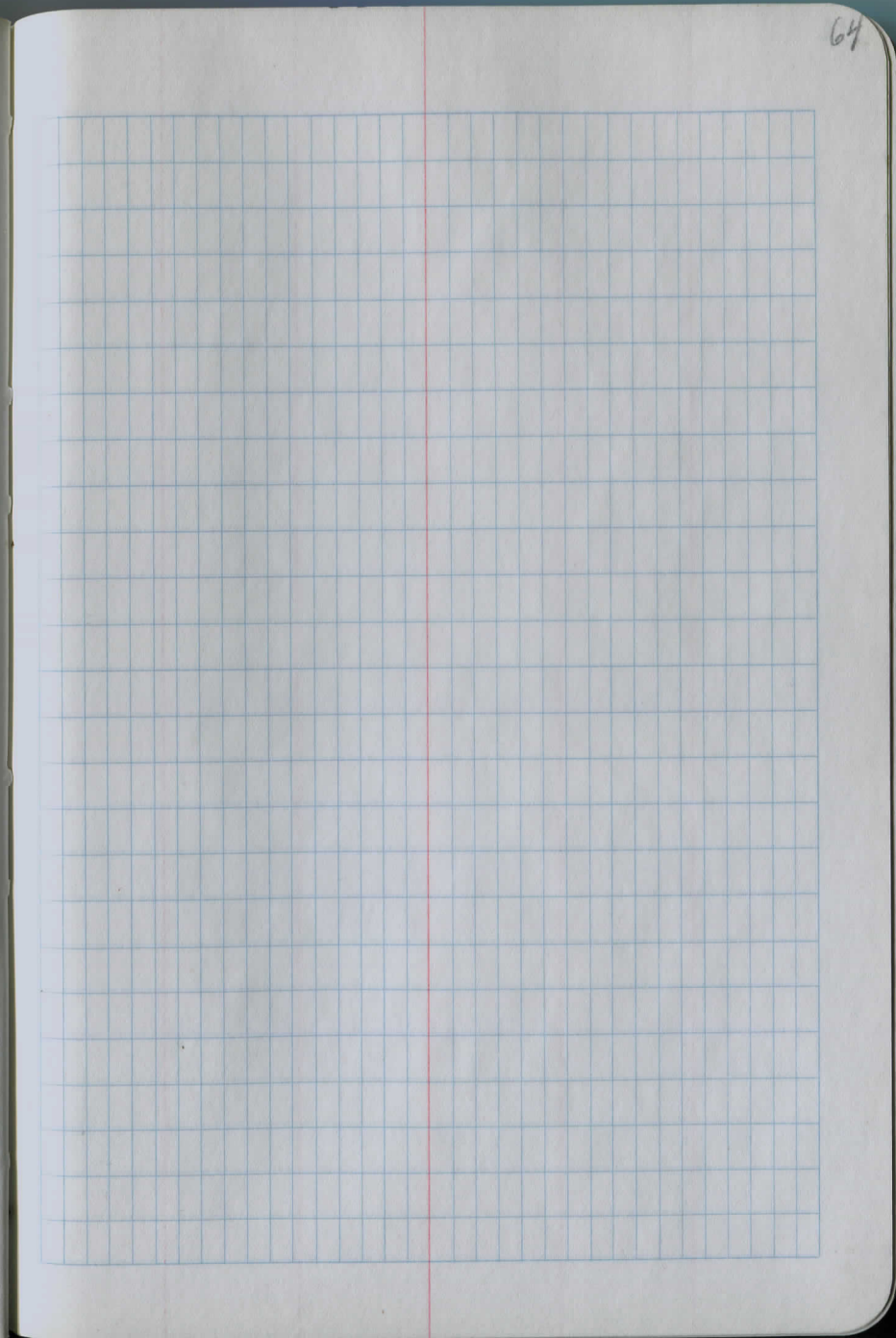
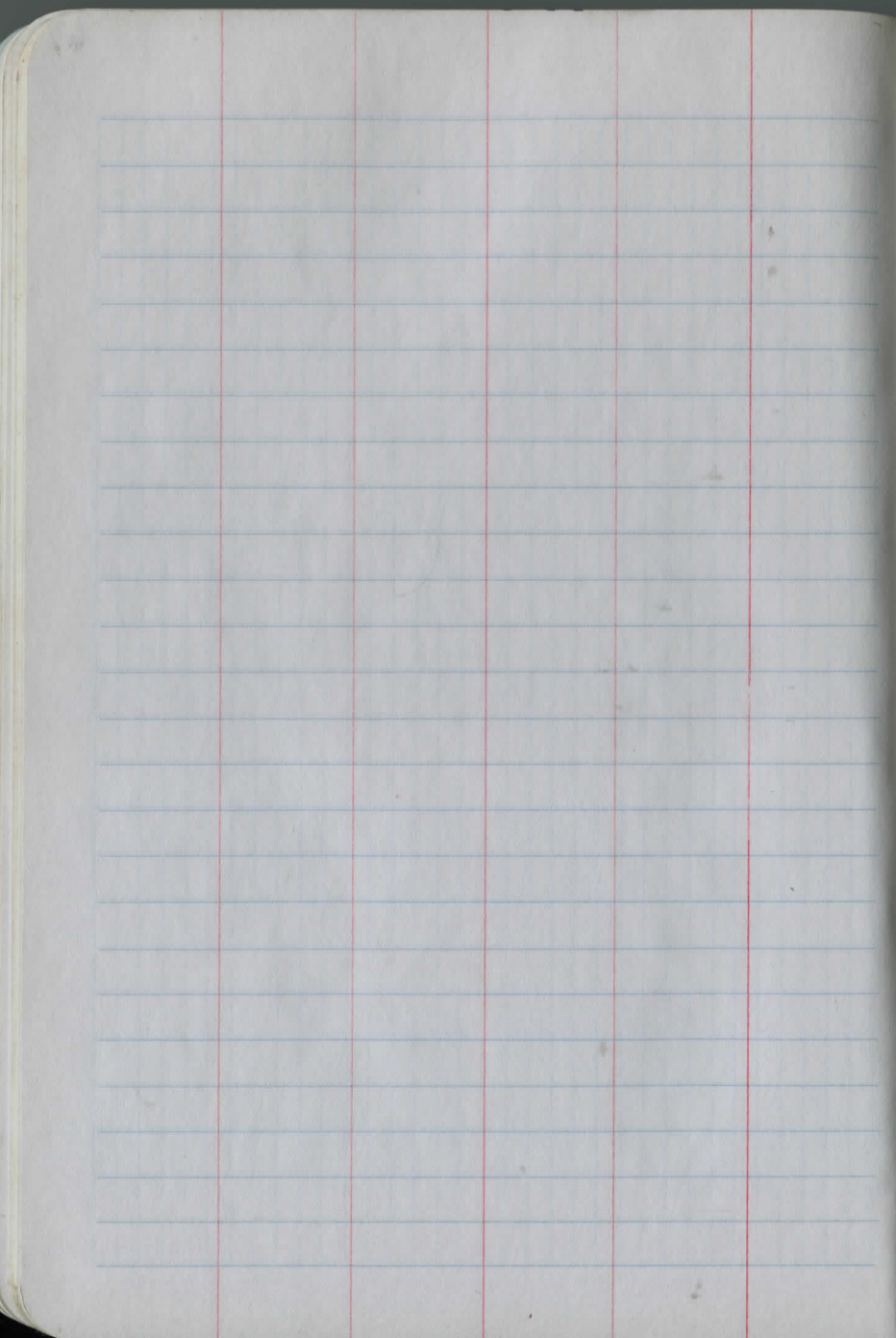


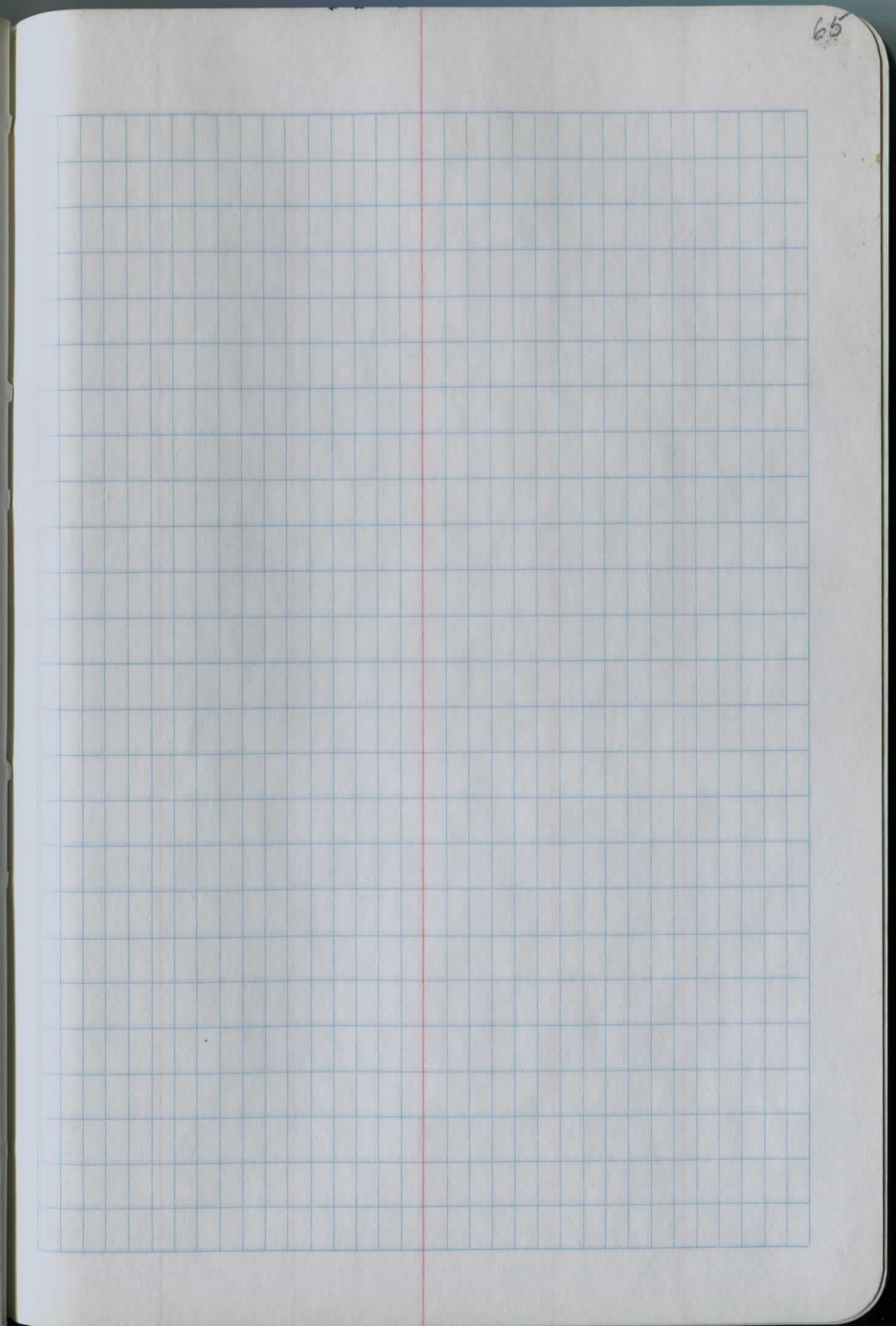
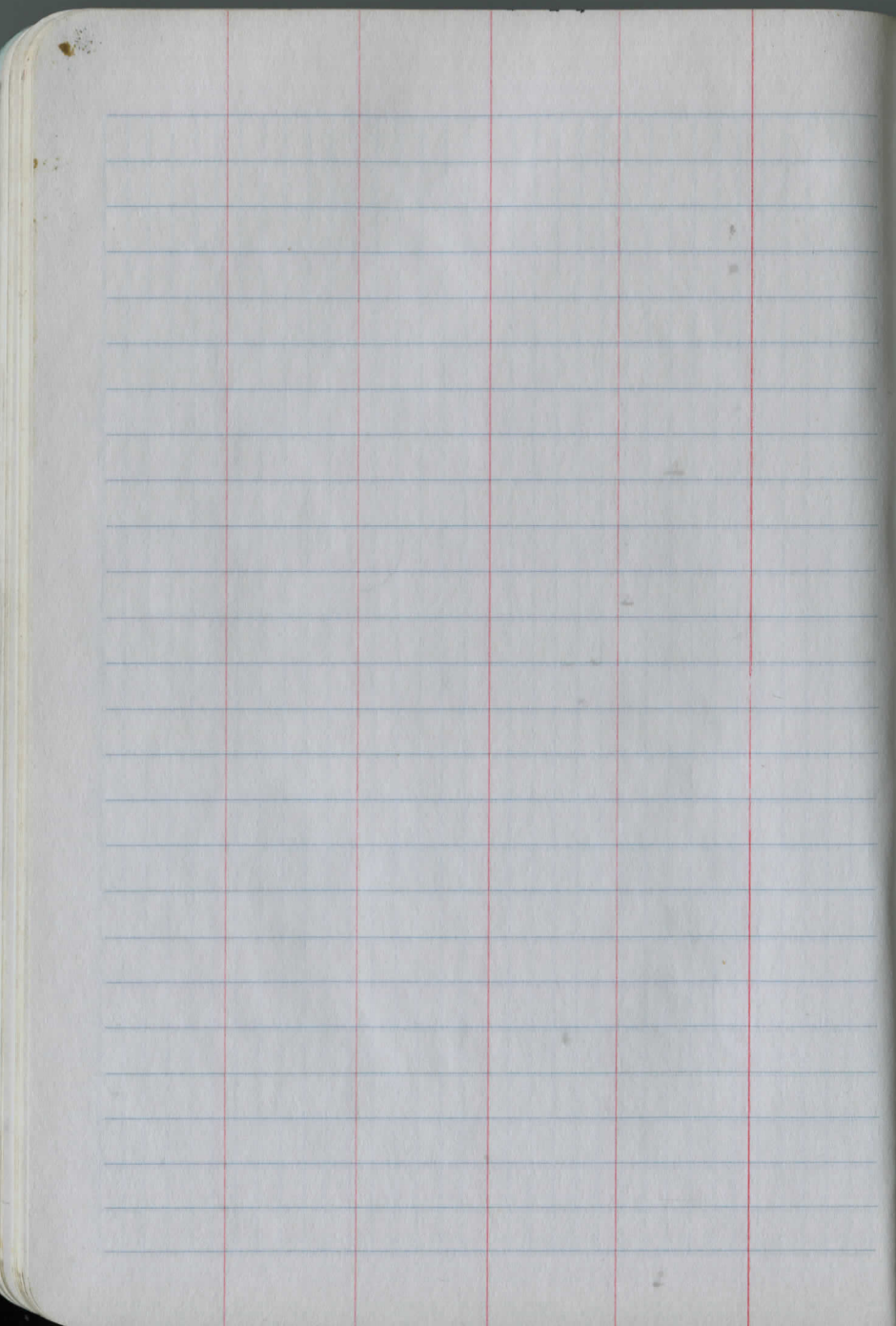


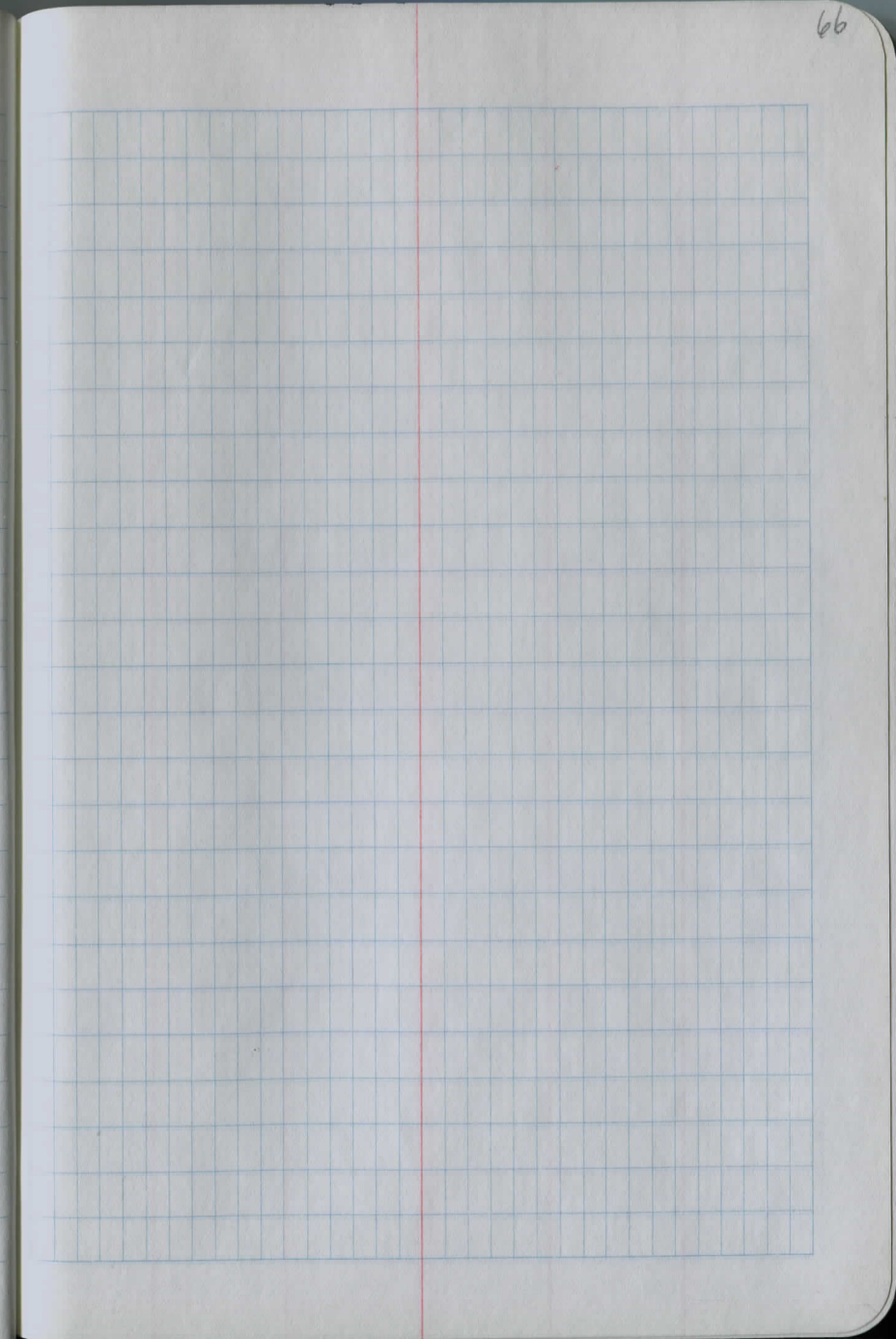
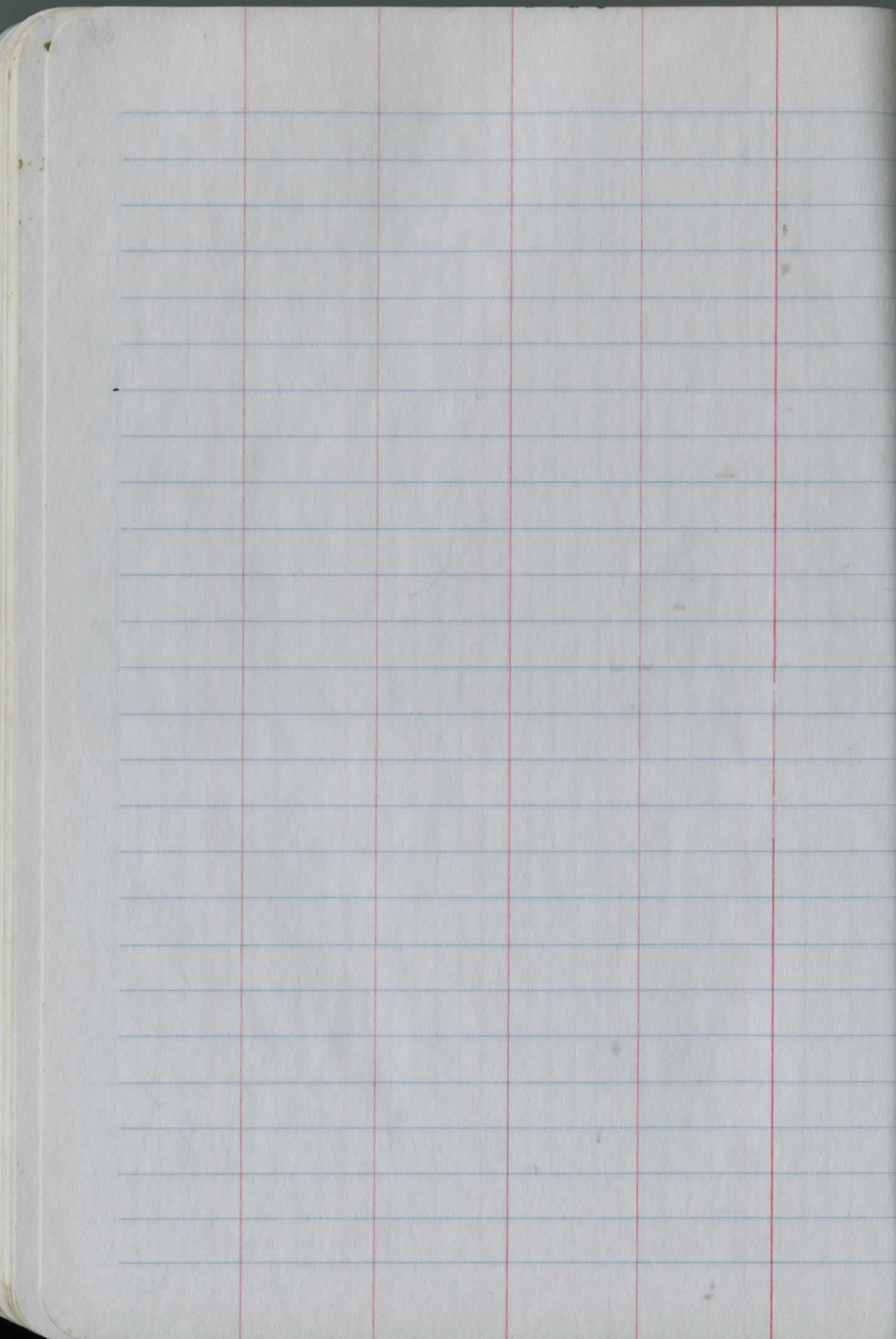


This page is a blank ledger with horizontal blue lines and four vertical red margin lines. The margins are located at approximately 10%, 20%, 80%, and 90% of the page width from the left edge.

This page is a blank ledger with a grid of blue lines and one vertical red margin line. The margin is located at approximately 10% of the page width from the left edge. The grid consists of 20 columns and 25 rows.







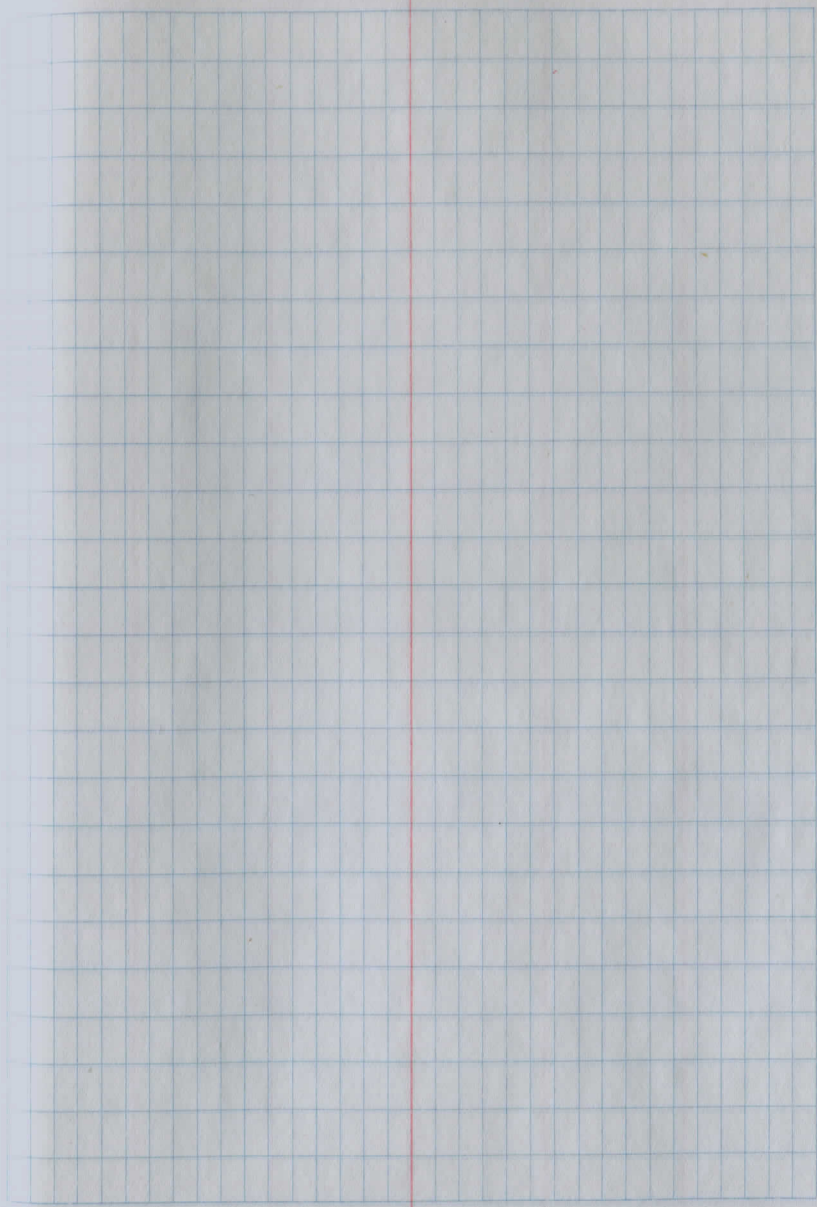
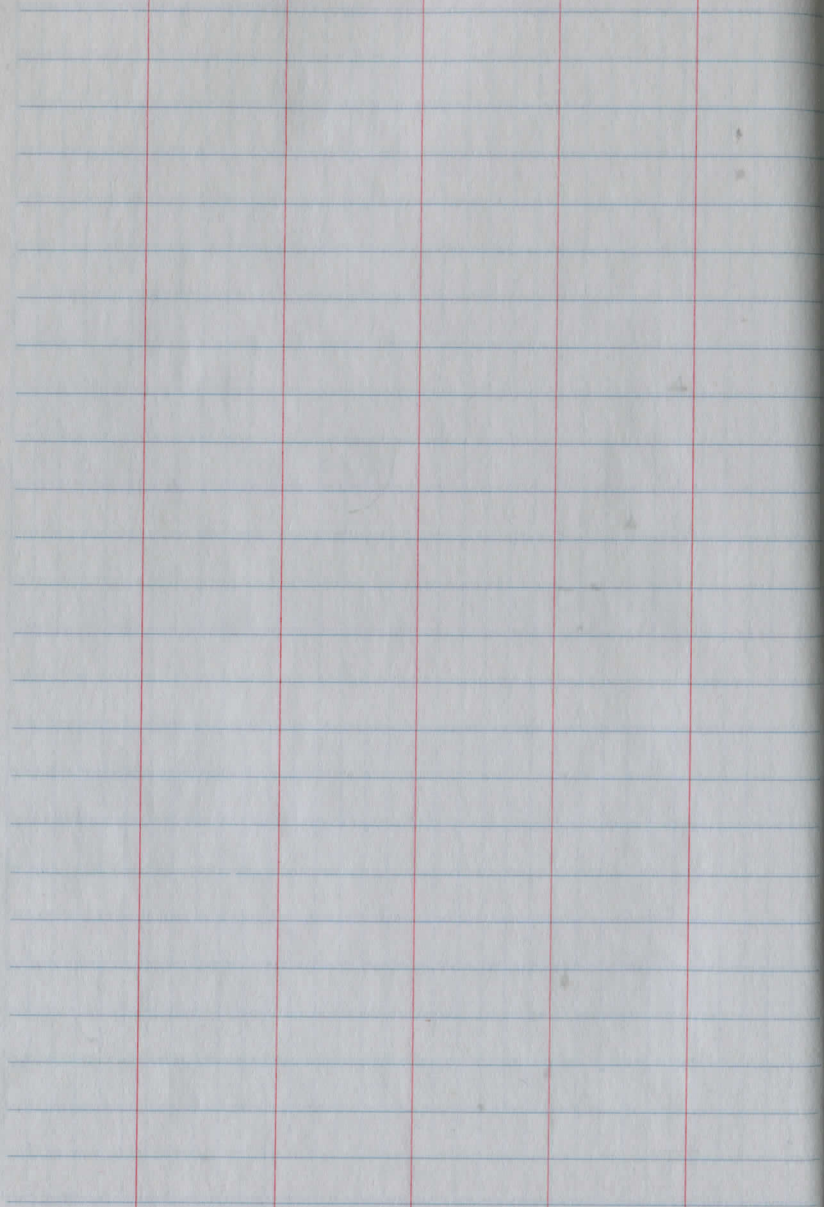
This page is a blank ledger sheet. It features a series of horizontal blue lines spaced evenly down the page. Four vertical red lines are drawn across the page, creating five columns of varying widths. The columns are roughly in the proportions of 1:1:1:1:2 from left to right. The page is otherwise empty of any text or markings.

This page is a blank ledger sheet with a grid layout. It has a vertical red line near the left edge, creating a narrow left margin. The rest of the page is filled with a grid of blue lines, forming a table with 15 columns and 25 rows. The page is otherwise empty of any text or markings.



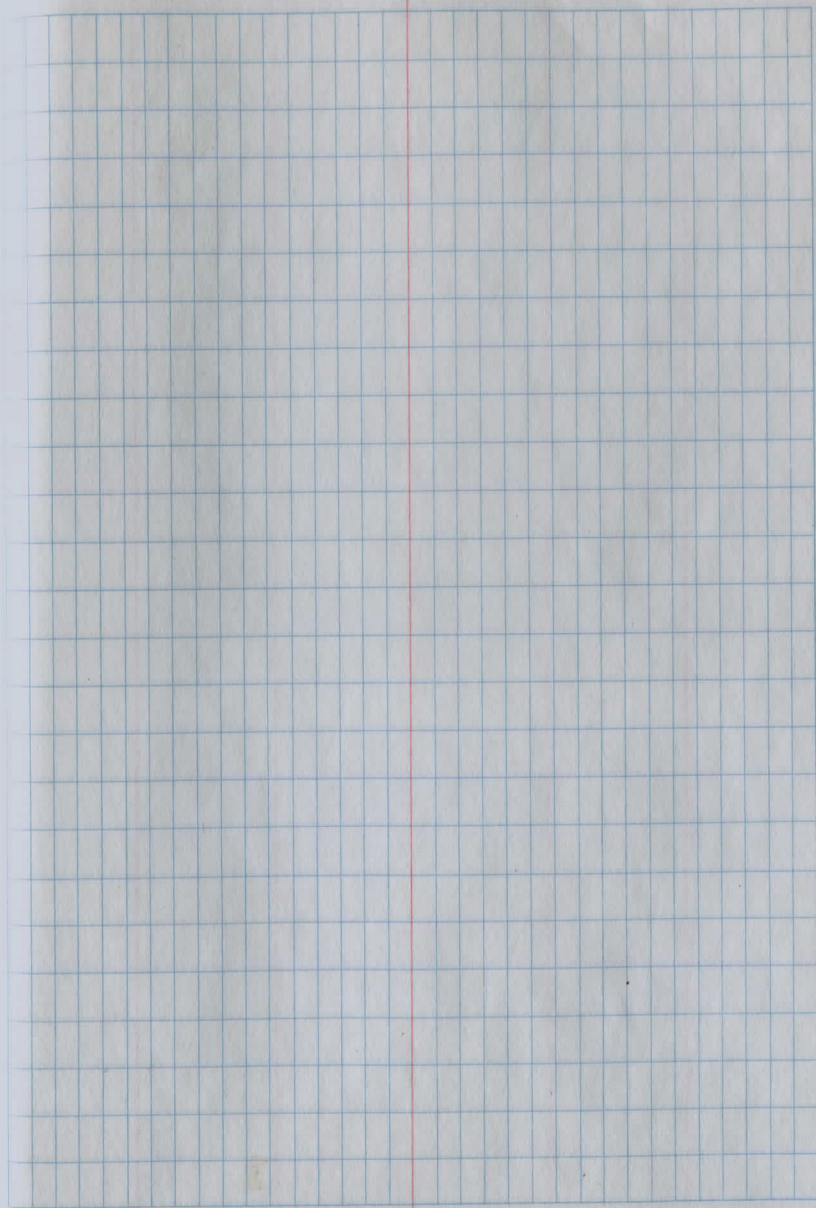
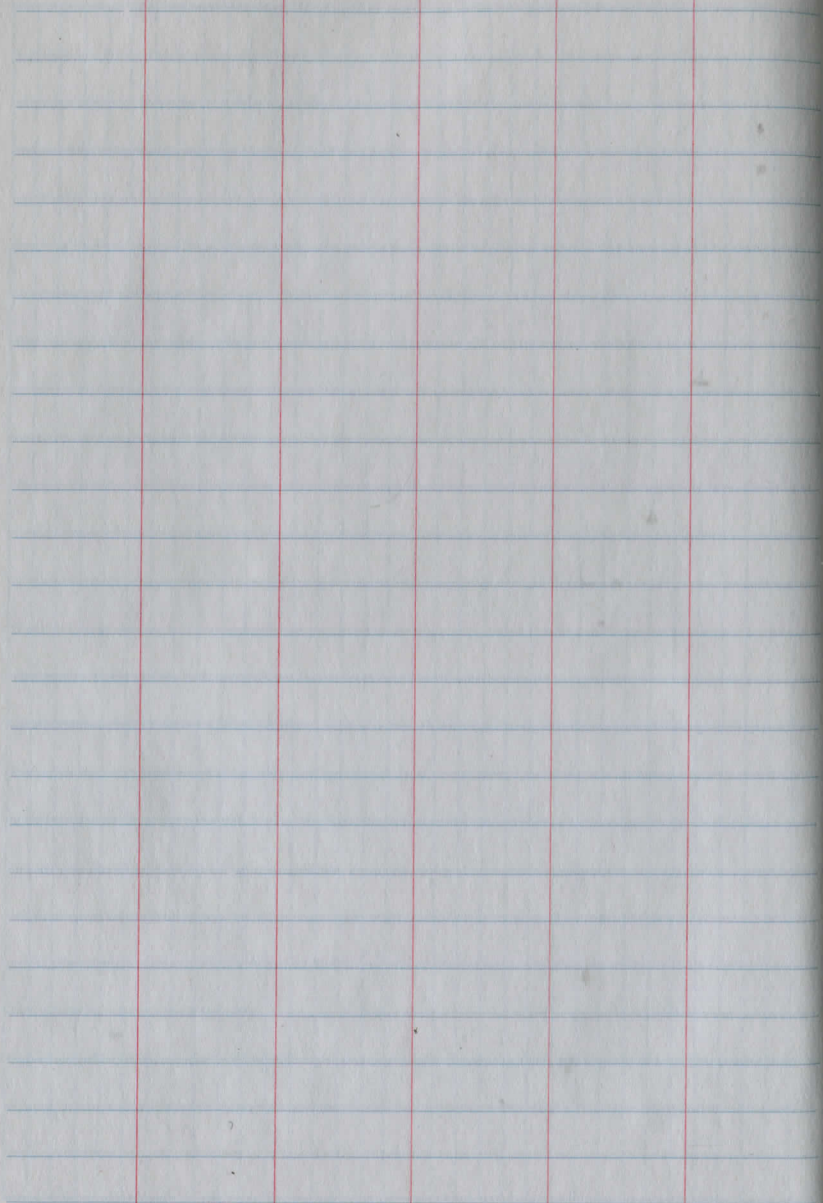
This page is a blank ledger with horizontal blue lines and three vertical red margin lines. The margins are located at approximately 12%, 20%, and 38% from the left edge of the page.

This page is a blank ledger with horizontal blue lines and a vertical red margin line at approximately 38% from the left edge. The right portion of the page is filled with a grid of small squares, typical of a ledger for recording transactions.



Blank lined page with three vertical red margin lines.

Blank grid page with a vertical red margin line.

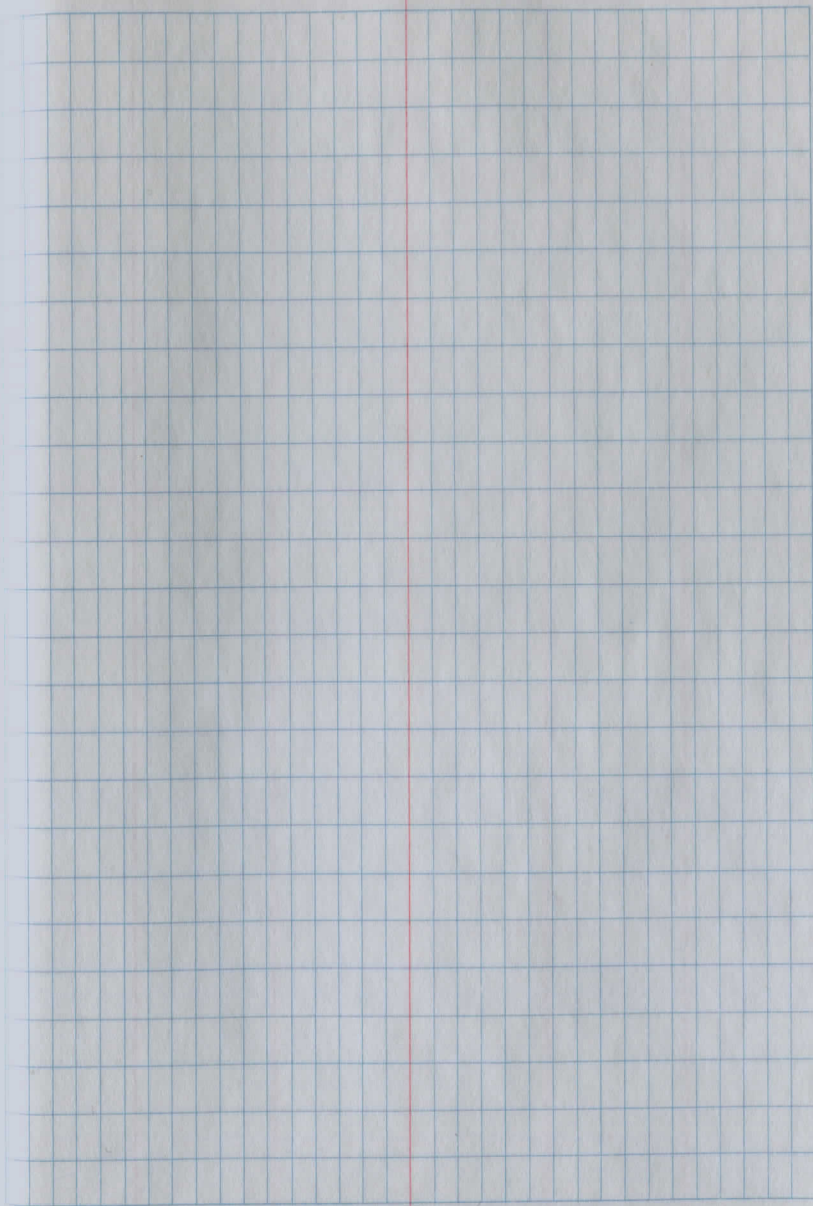
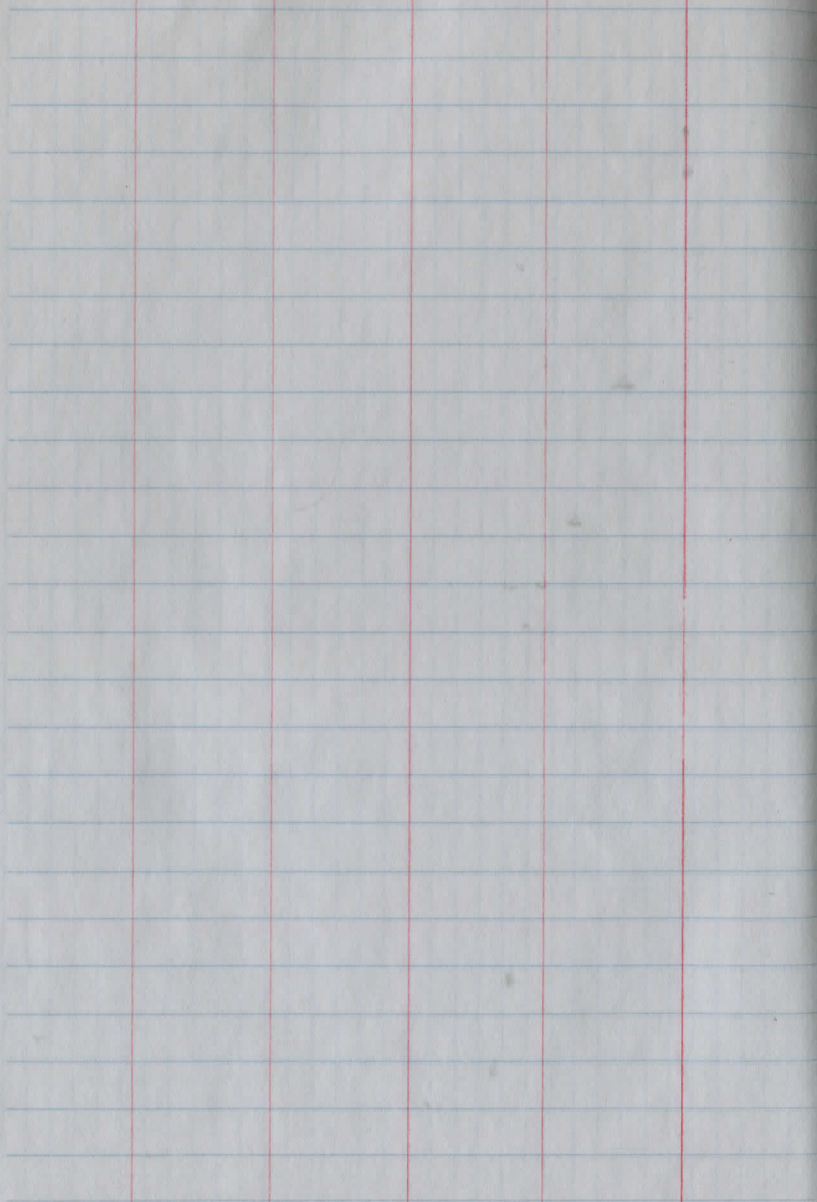


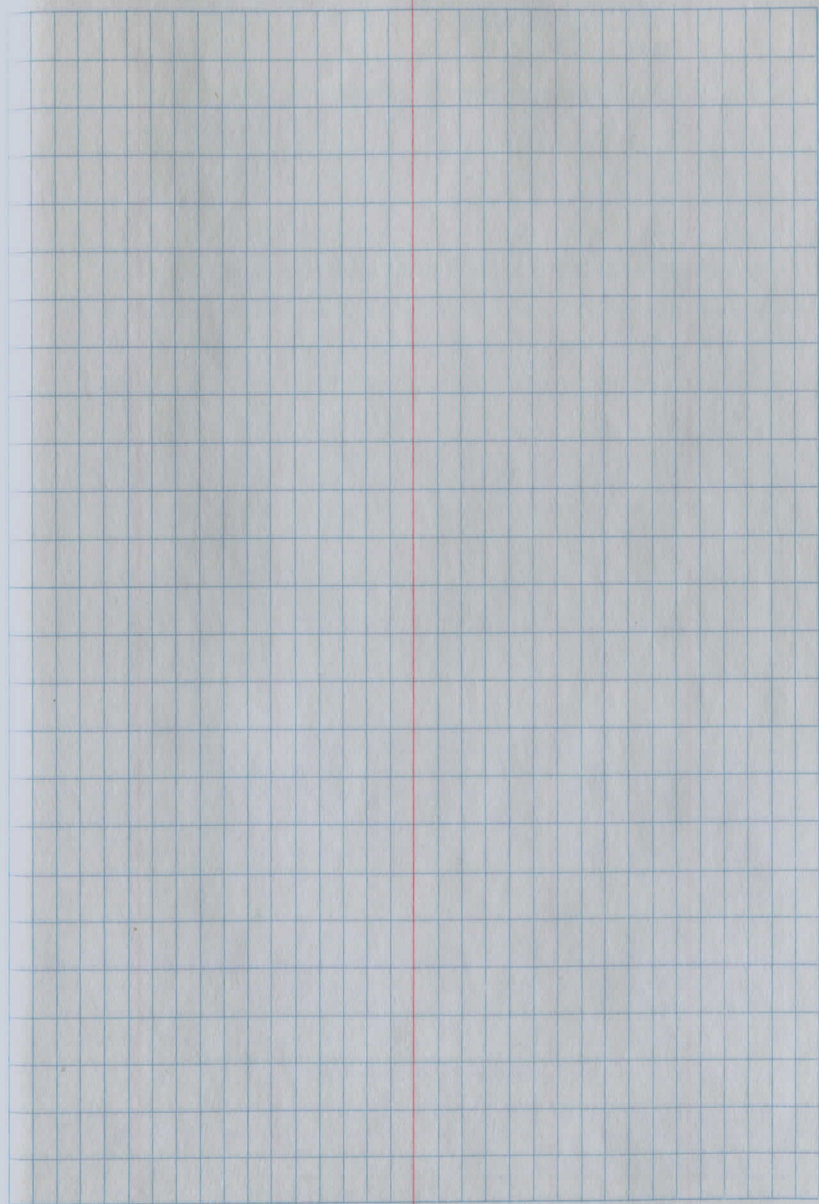
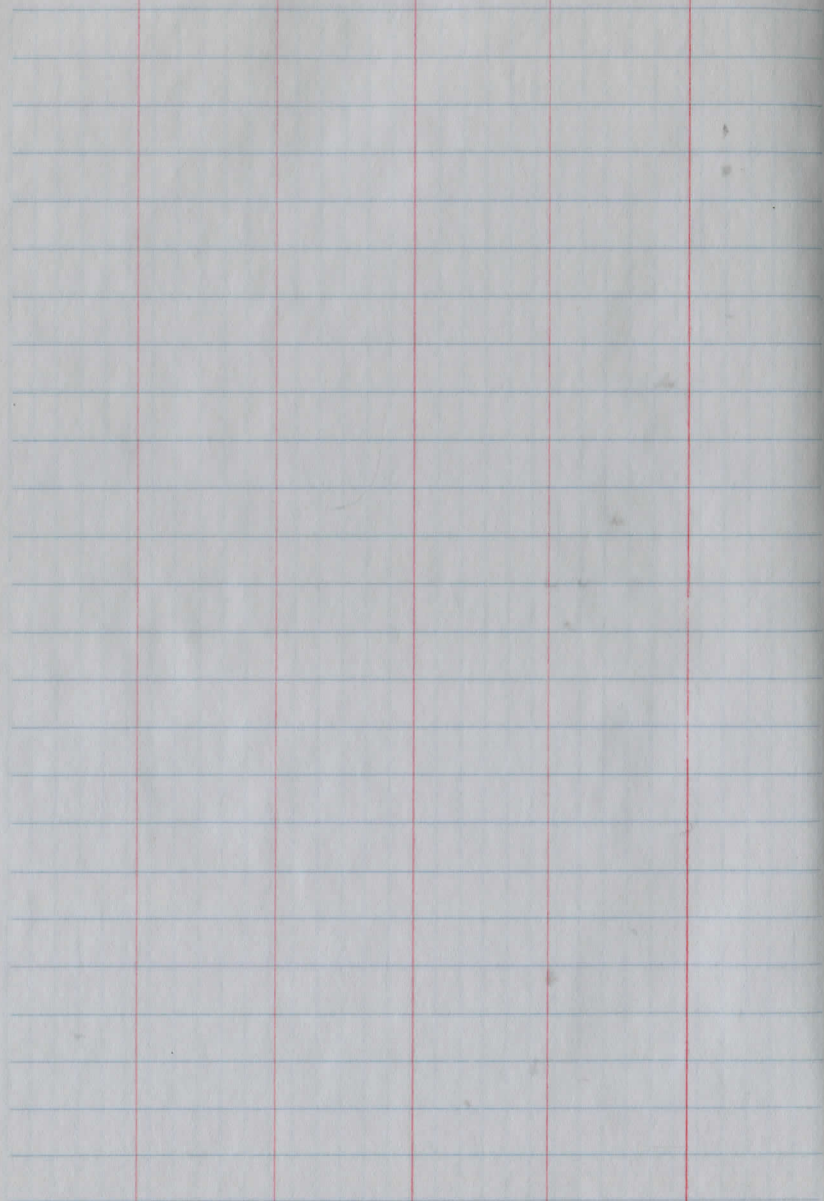
Blank lined page with three vertical red margin lines.

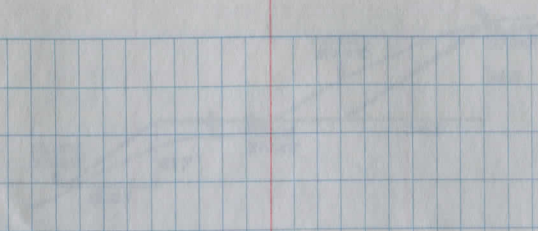
Blank grid page with a vertical red margin line.

Blank lined page with horizontal blue lines and three vertical red margin lines.

Blank grid page with a grid of blue lines and one vertical red margin line.







Handwritten text, possibly a title or description, located below the sketch. The text is very faint and difficult to read, but appears to be a single line of writing.

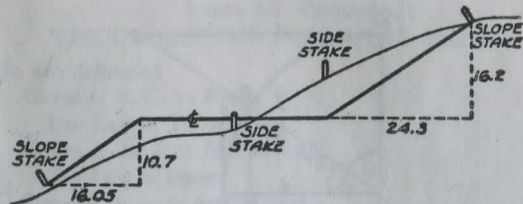


TABLE I.—DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.60	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.60	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

TABLE No. 1

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

PLEASE RETURN TO  
GEAUGA COUNTY ENGINEER  
COURT HOUSE  
CHARDON, O.  
PHONE 250-X

15-21

164-39  
329-19  
133-59

926  
1089.22<sup>m</sup> = ctr Spk  
6.57  
1095.79

